



# Transmission Expansion Advisory Committee

May 12, 2010



# Issues Tracking

- Issues requested at April PC/TEAC meeting
- Responses received
  - Administrative questions (TEAC meeting minutes)
  - Local planning discussion
  - Cost allocation (post projected cost allocations to the web)
- Issues tracking related to outstanding analytic questions / needs

Owner	Requestor	Issue Identifier	Issue Title	Issue Description	Issue Status	Stakeholder Body	Date Created
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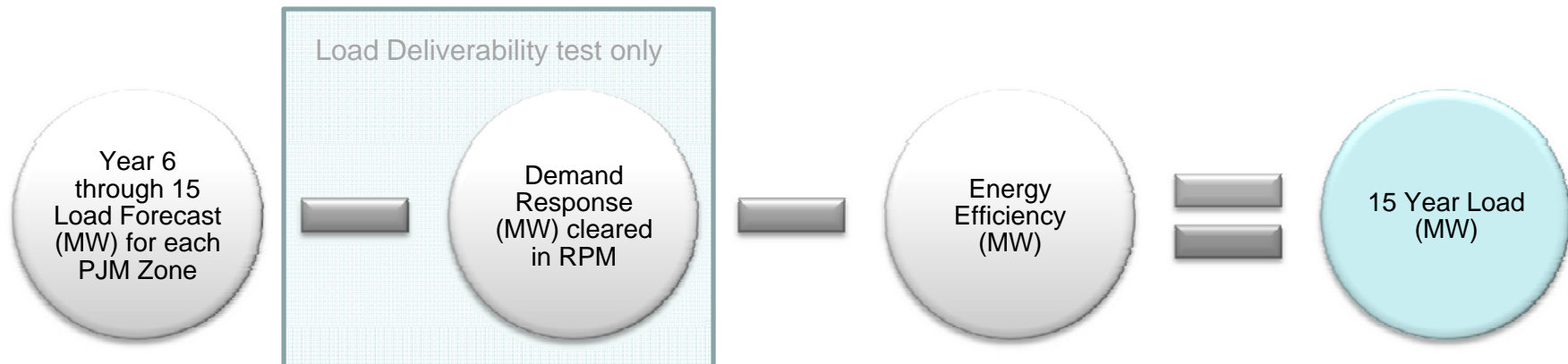


## 2010 RTEP Sensitivity Analysis Methodology

- Analysis will focus on EHV facilities
- Studies will focus on long term impact

- Yearly Load Increase (MW) for each PJM Zone
  - Difference in Yearly Load Forecasts for each PJM Zone
- Area Load DFAX (p.u.) for each PJM Zone
  - Source = all PJM generation
  - Sink = load in each PJM zone
- Existing Demand Response and Energy Efficiency
  - Reflected in the Yearly Load Increase

- 15 Year Load (MW) Calculation including existing DR & EE
  - Calculated for years 6 through 15 for each PJM zone



- **15 Year Loading Multiplier**
  - Calculated for years 6 through 15 for every facility
  - Scales the loading to include the impact of supplying additional load in a future year



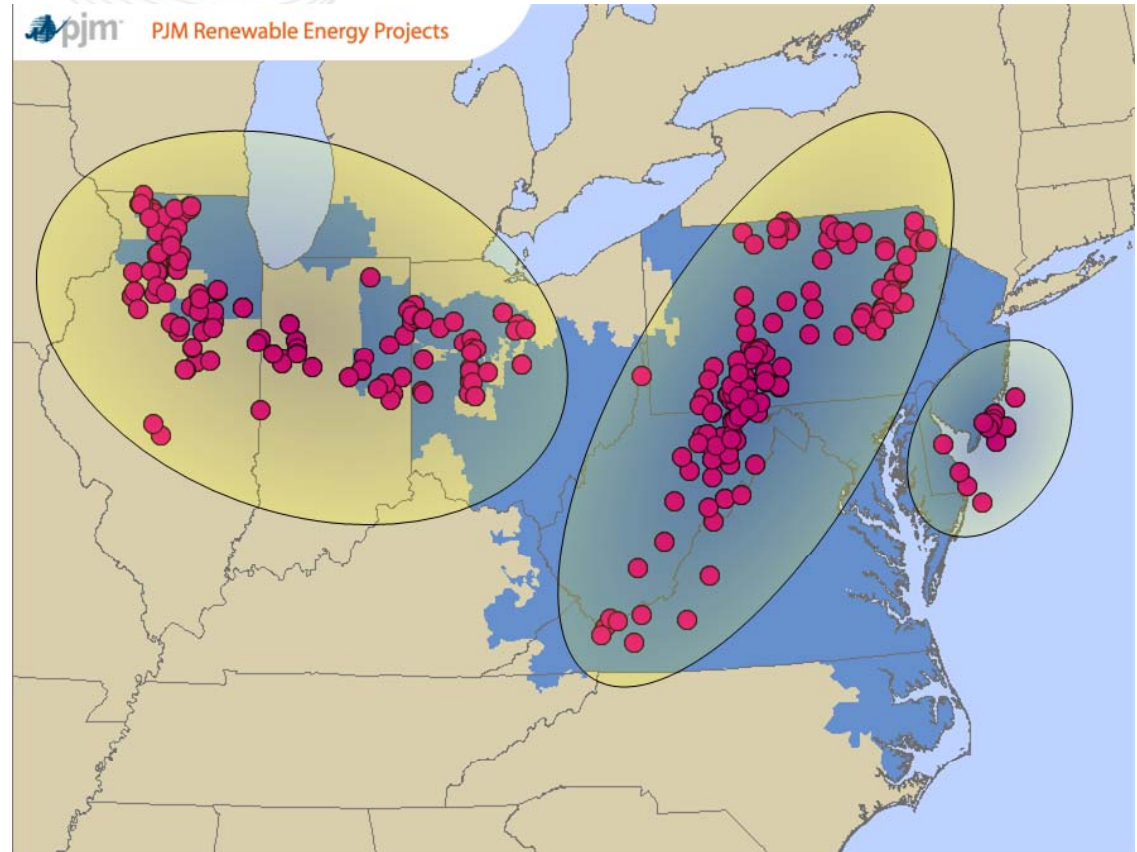


- Final 15 Year Loading (%)
  - 15 year loading (MW) / Facility Rating
  - Calculated for years 6 through 15 for every facility



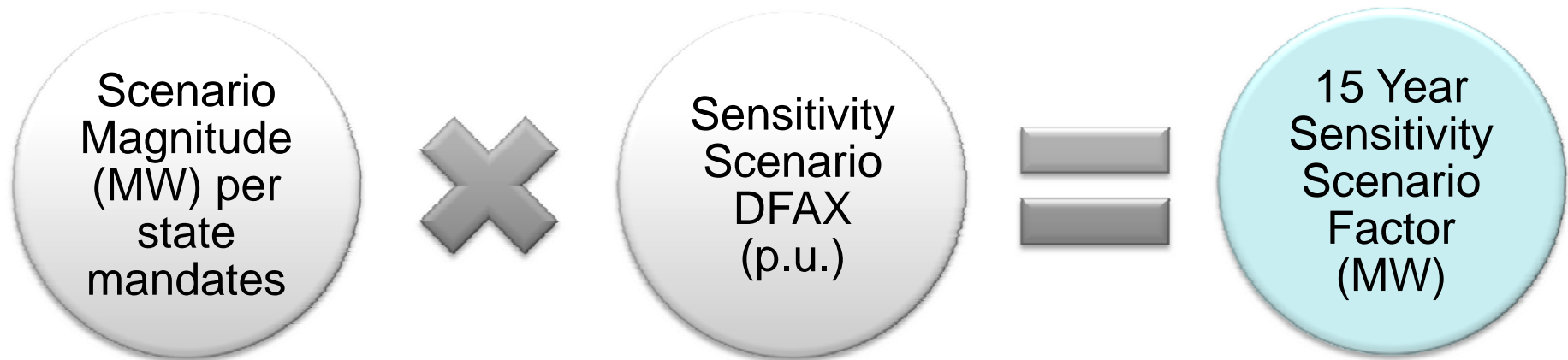
## 15 Year Calculations (Sensitivity Analysis Method)

- Source used for Sensitivity Scenario DFAX calculation
  - Three zones
    - Atlantic Offshore
    - Appalachian Mountains
    - Western
  - Buses selected from each zone for use in DFAX calculation
  - Participation factor for each zone calculated using existing interconnection queue data



- Sink used for Sensitivity Scenario DFAX calculation
  - Scenario Dependant
    - Assume existing PJM generation remains
      - Sink = all PJM generation
    - Assume at-risk generation is displaced
      - Sink = at-risk generation
  - At-risk generation
    - Generation that has not cleared in recent RPM auctions
    - Generation in a carbon constrained world
    - Revenue adequacy at risk generation
      - MMU SOM report identified 11,250 MW of generation
    - Aging Generation

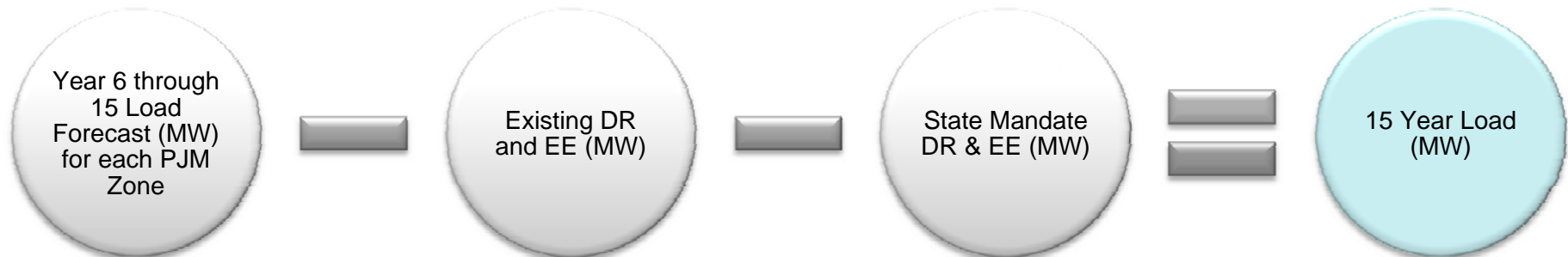
- **15 Year Sensitivity Scenario Factor**
  - Calculated for years 6 through 15 for each PJM zone
  - DFAX calculated by sourcing wind generation and sinking to at-risk generation
  - Sensitivity scenario magnitude calculated using state RPS requirements



- **Final Sensitivity 15 Year Loading (%)**
  - Final loading (MW) / Facility Rating
  - Calculated for years 6 through 15 for every facility



- 15 Year Load (MW) including existing DR & EE and state DR & EE mandates
  - Calculated for years 6 through 15 for each PJM zone



1. Add renewable generation to meet RPS assuming existing PJM generation remains
2. Add renewable generation to meet RPS assuming RPS displaces at-risk generation
3. Add renewable generation to meet RPS + DR + EE mandates assuming RPS displaces at-risk generation

Scenario	Sensitivity	Source	Sink	Test
RPS Sensitivity 1	RPS	Renewable Generation	Existing PJM Generation	Generator Deliverability & Load Deliverability
RPS Sensitivity 2	RPS	Renewable Generation	At-Risk Generation	
RPS Sensitivity 3	RPS + DR + EE	Renewable Generation	At-Risk Generation	



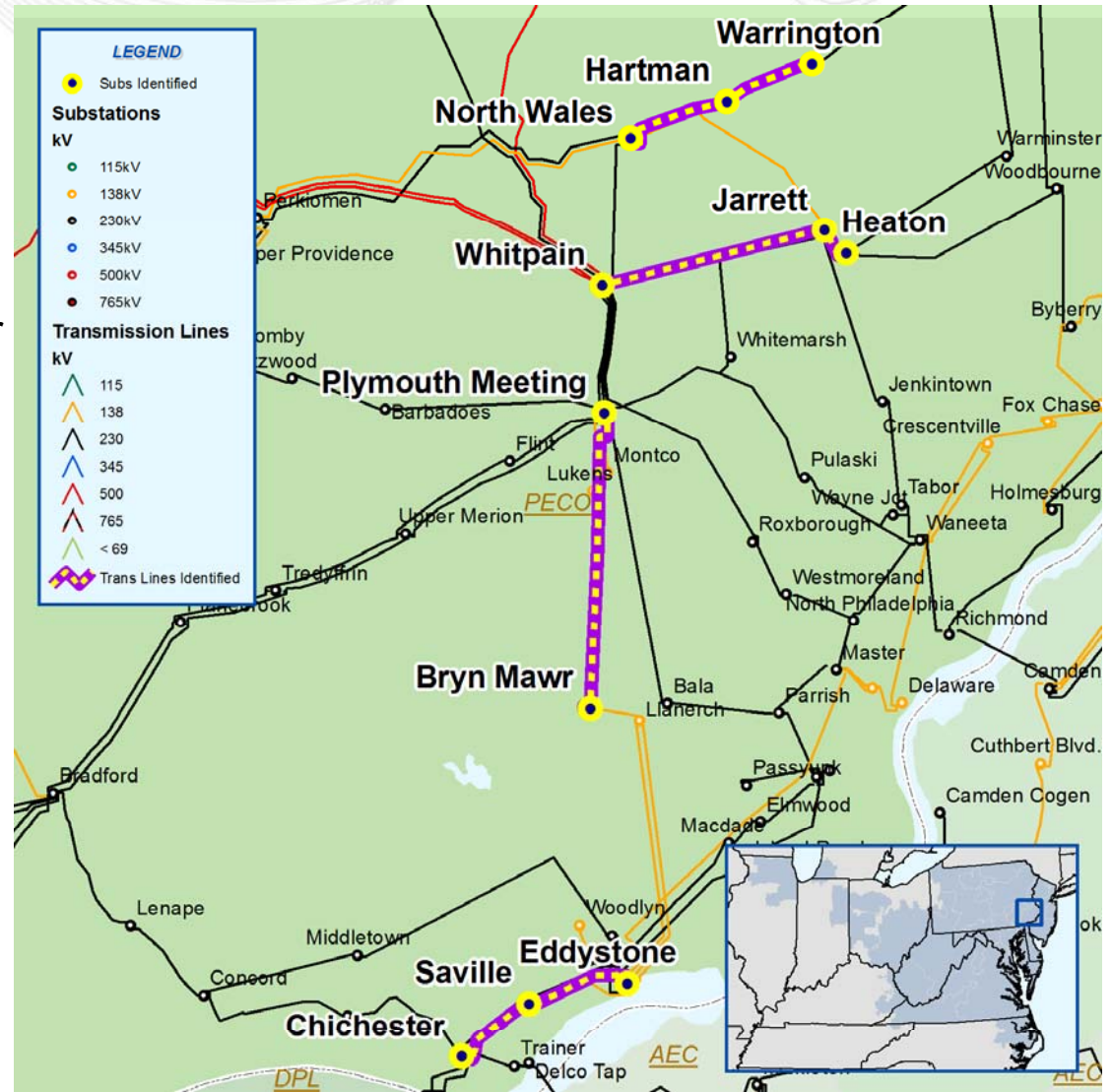
# Eddystone & Cromby Retirement Study Update\*

\* Indicates updated information since March 2010 TEAC Meeting

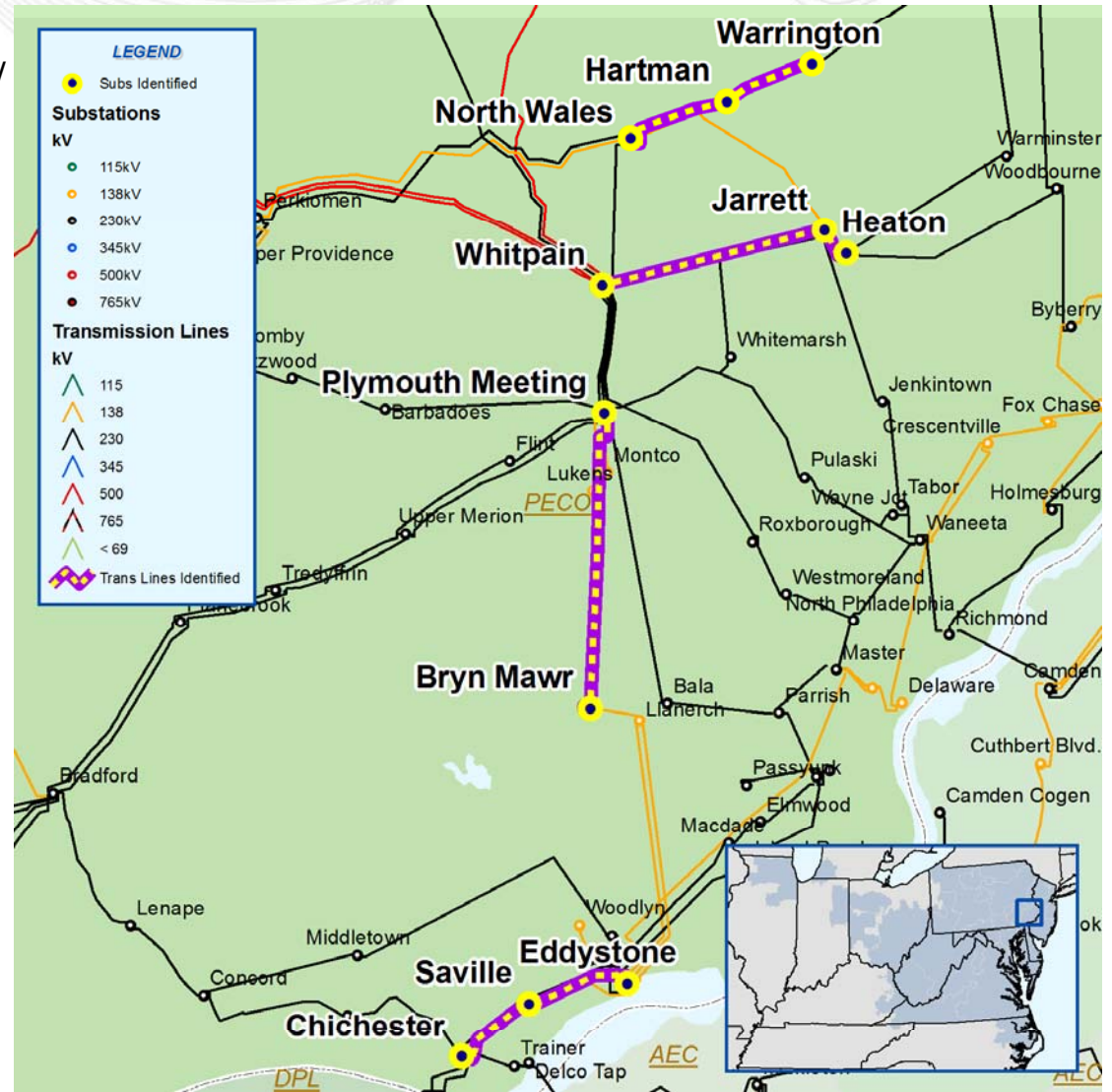


- In December 2009 Exelon notified PJM of their intent to retire the Eddystone 1&2 units and the Cromby 1&2 units in the PECO Energy Transmission zone
- Proposed deactivation date is May 31, 2011
- PJM staff has been evaluating the impact of the proposed deactivation
- The following slides include the recommended upgrades and the expected in-service date

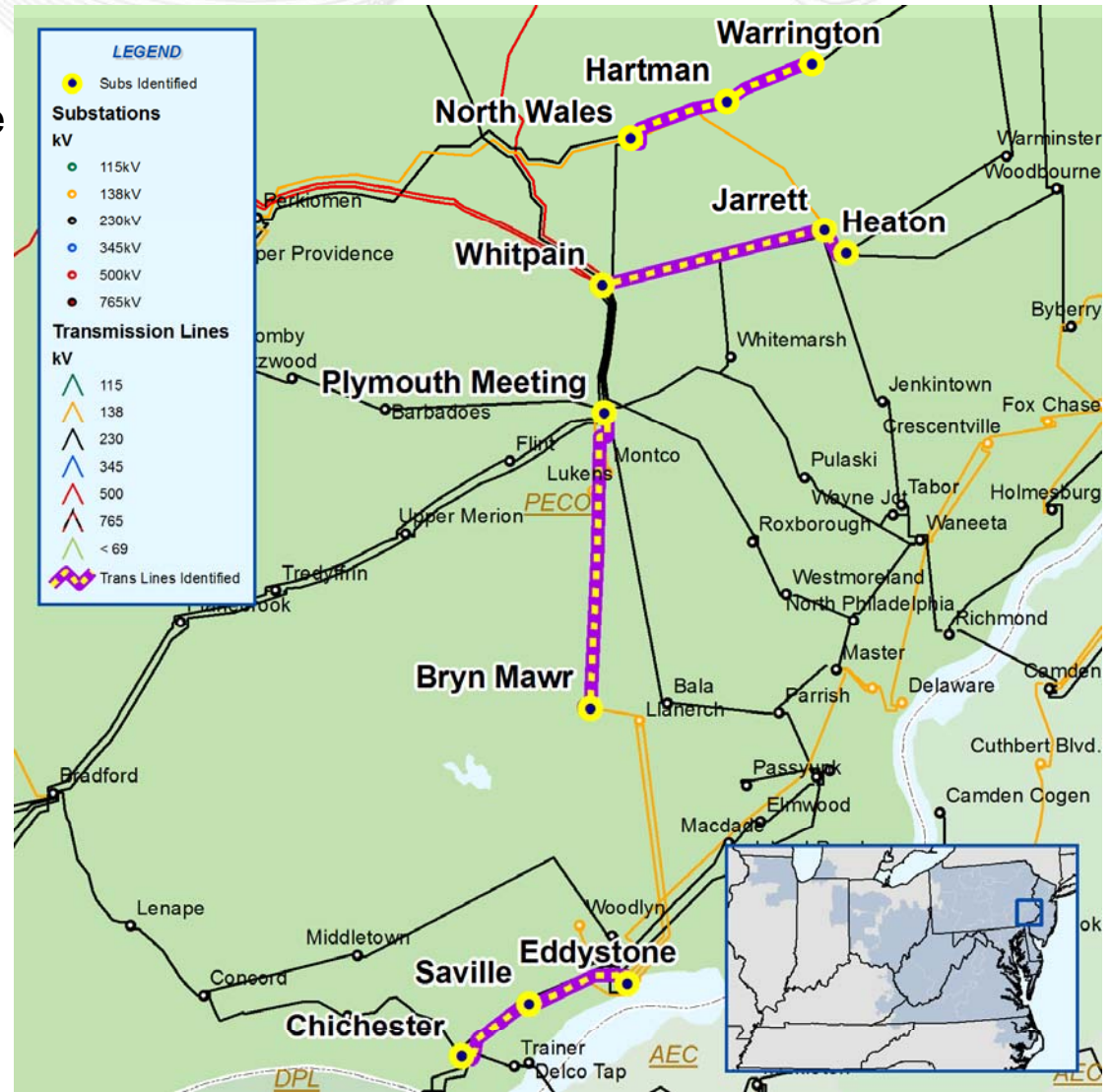
- Chichester 230/138 kV transformer / loss of Macdade – Ridley – Morton 230 kV line (220-46) + loss of Island Road – Eddystone 230 kV line (220-23)
- Recommended Solution: Add a second 230 / 138 kV transformer at Chichester. Add an inductor in series with the parallel transformers
- Estimated cost: \$5.908 M
- Expected In-service: December 16, 2011



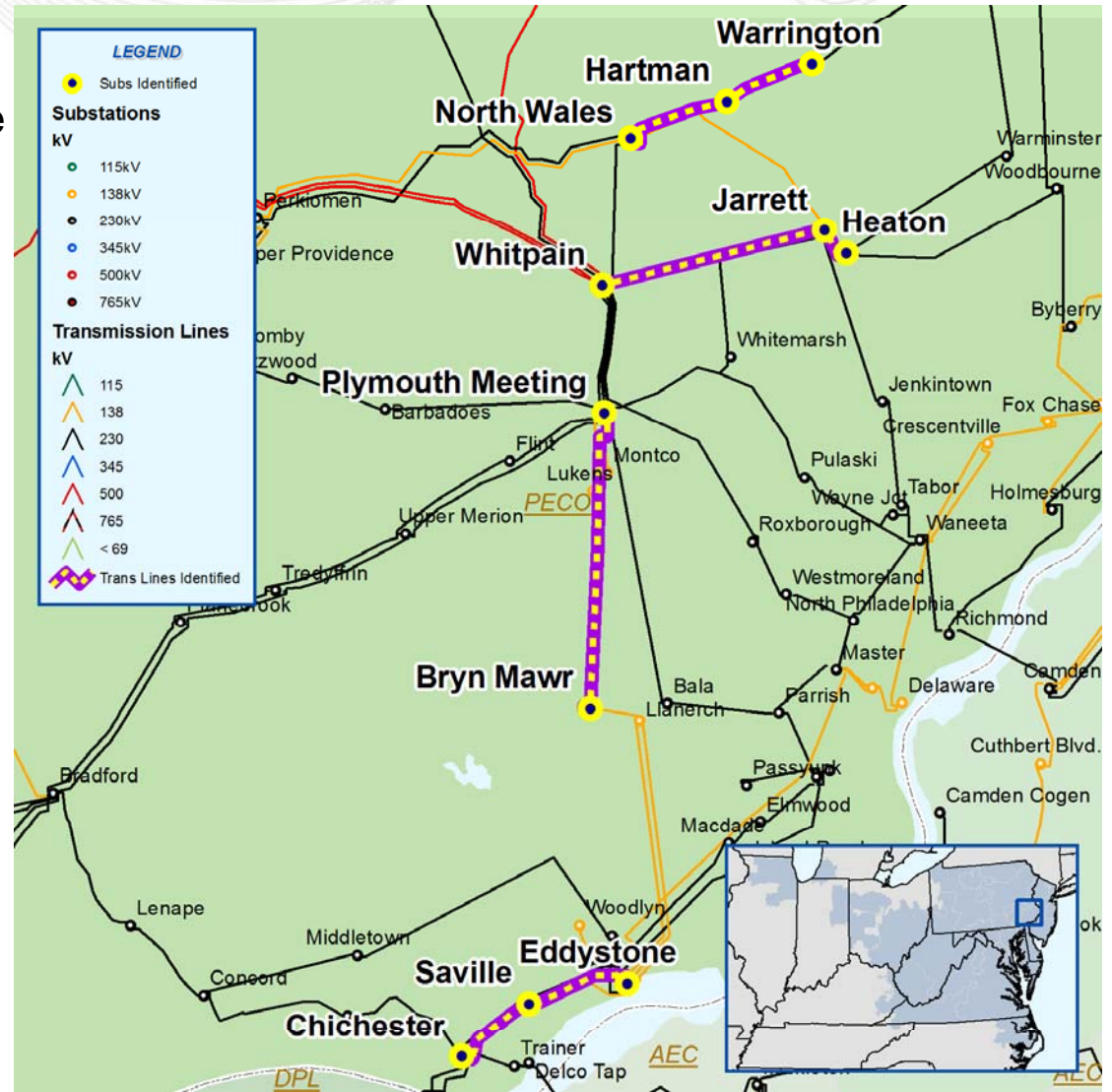
- Eddystone – Saville 138 kV line / loss of Macdade – Ridley – Morton 230 kV line (220-46) + loss of Island Road – Eddystone 230 kV line (220-23)
- Recommended Solution: Replace terminal equipment at Eddystone and Saville and replace underground section of the line
- Estimated Cost: \$3.94 M
- Projected In-Service: May 27, 2011



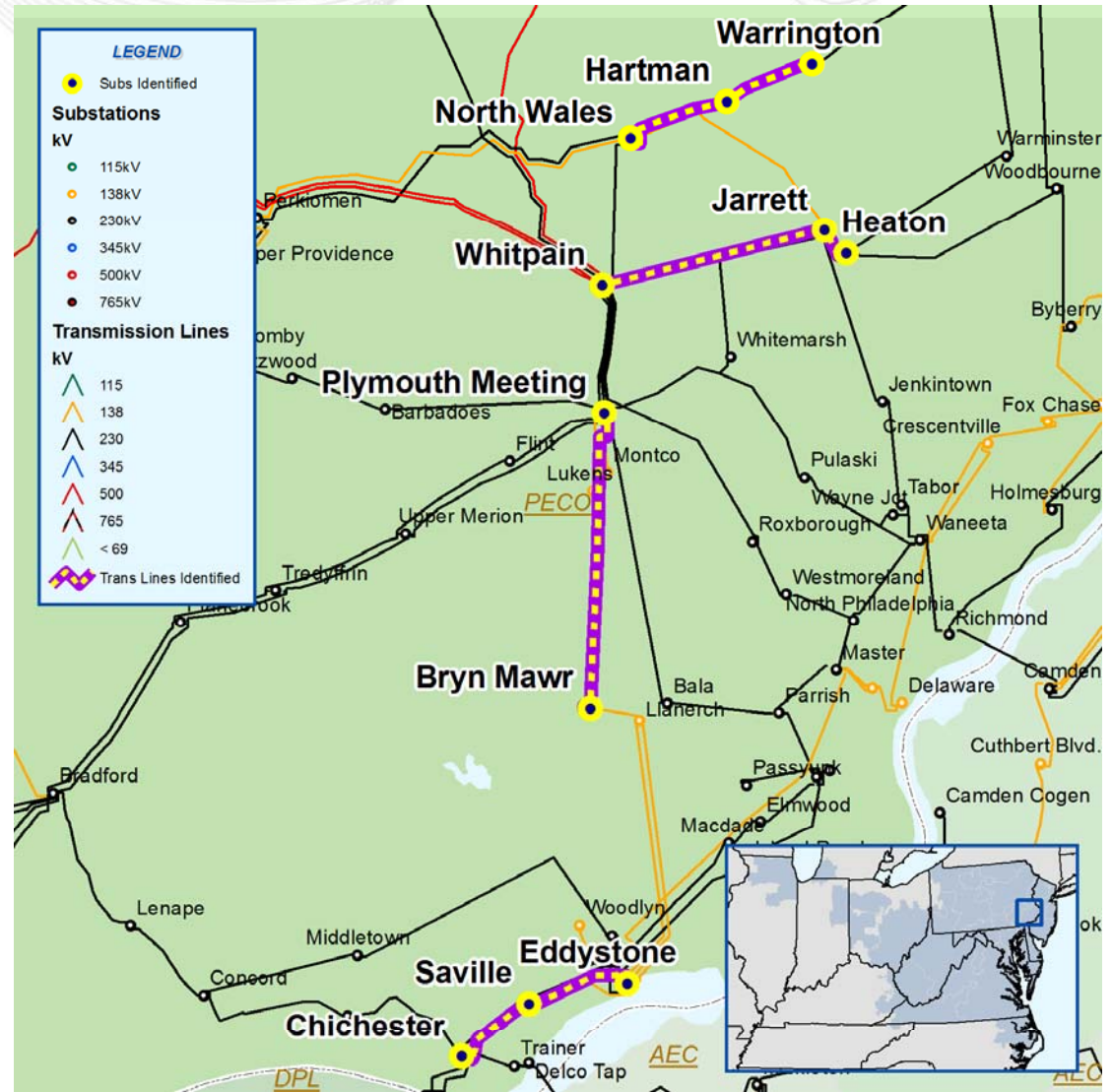
- Jarrett – Whitpain 230 kV line / loss of North Wales – Hartman 230 kV line (220-71) + Basecase
- Recommended Solution: Replace terminal equipment at Whitpain and Jarrett
- Estimated Cost: \$ 0.175 M
- Projected In-Service: May 27, 2011



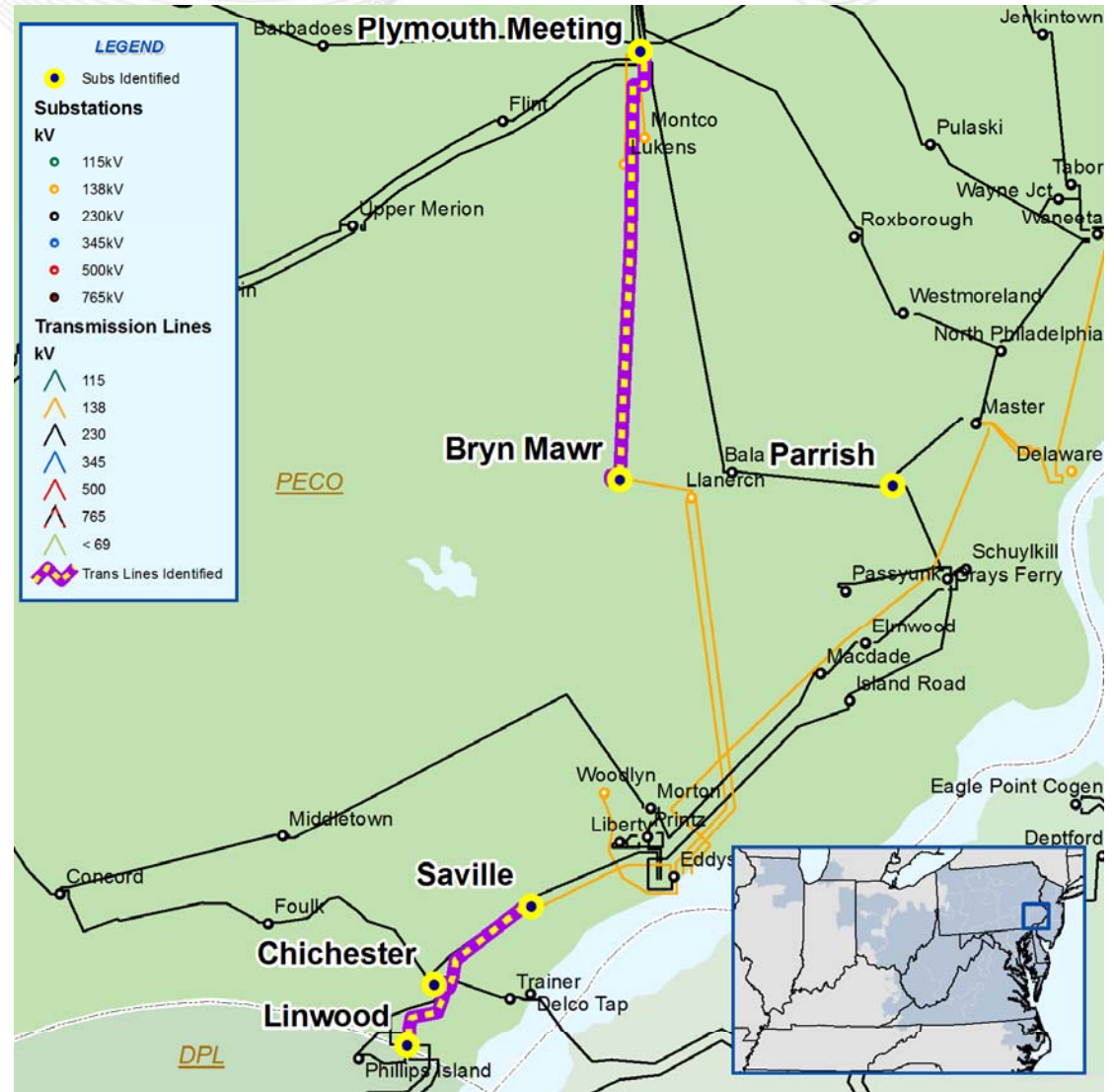
- Jarrett – Heaton 230 kV line / loss of North Wales – Hartman 230 kV line (220-71) + Basecase
- Recommended Solution: Replace terminal equipment at Heaton and Jarrett substations
- Estimated cost: \$ 0.525 M
- Expected In-Service: May 27, 2011



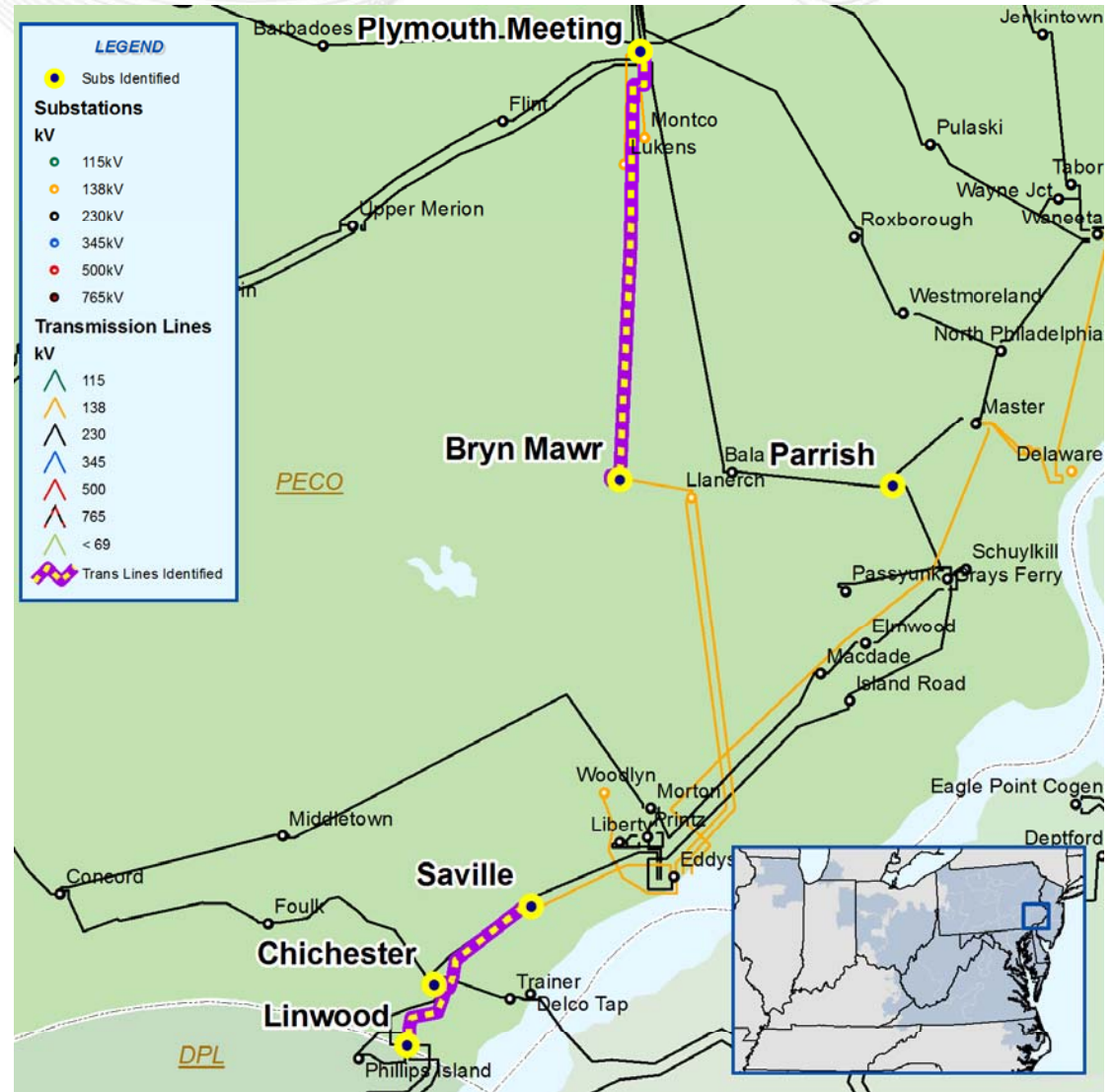
- Hartman – Warrington 230 kV line overload for the following contingencies
  - loss of Emilie – Neshaminy 138 kV line (130-25) + loss of Jarrett – Whitpain 230 kV line (220-52)
  - loss of Jarrett – Whitpain 230 kV line (220-52) + Basecase
- Recommended Solution: Replace terminal equipment at Warrington and Hartman
- Estimated Cost: \$ 0.375 M
- Projected In-Service: May 27, 2011



- Linwood – Chichester ‘220-43’ 230 kV line / single contingency (‘220-39’) loss of Linwood – Chichester ‘220-39’ 230 kV line and Phillips island generating units CT2, CT3, and ST
- Recommended Solution: Replace terminal equipment at Chichester
- Estimated Cost: \$0.475 M
- Expected In-Service: May 27, 2011

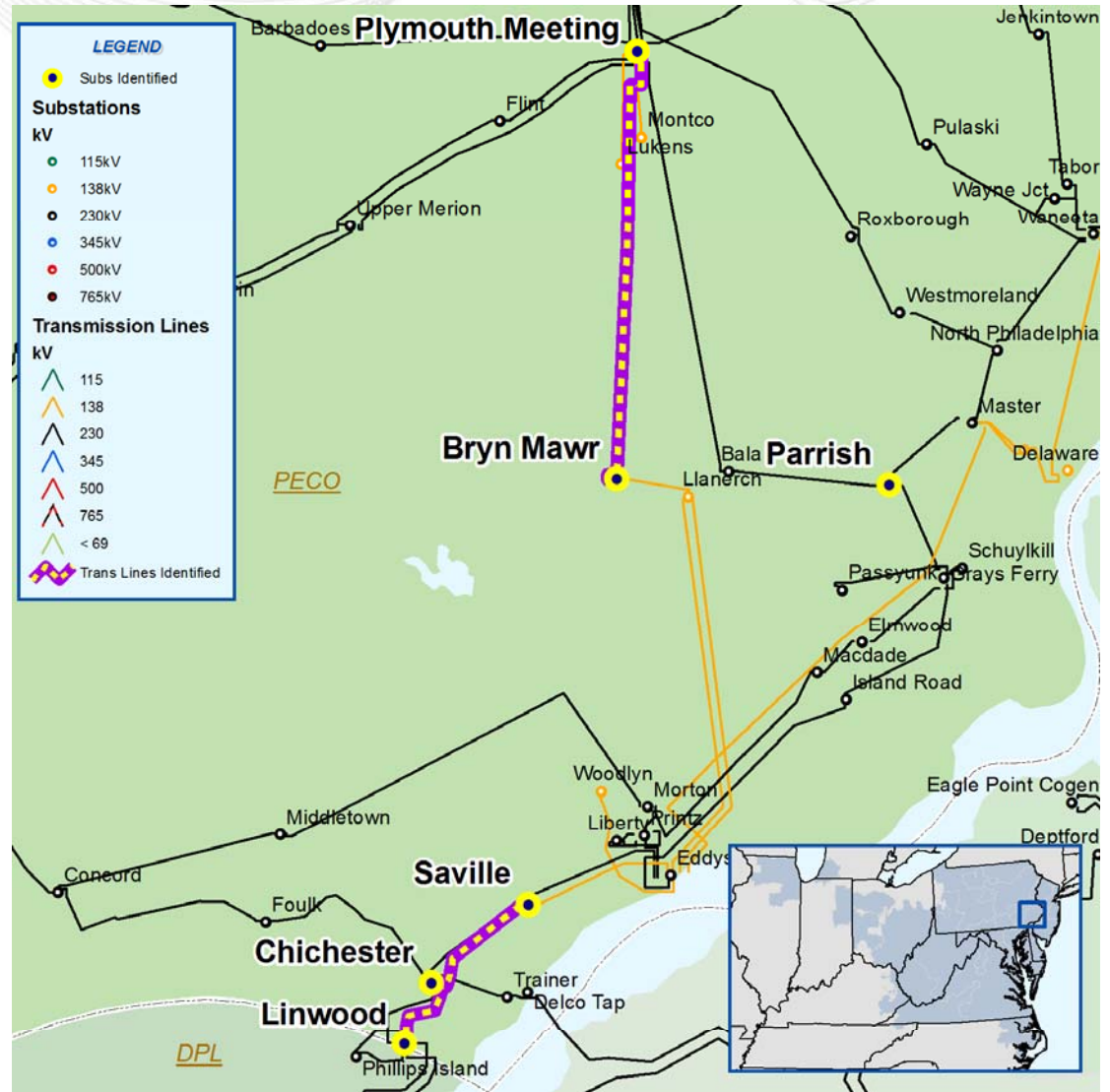


- Linwood – Chichester ‘220-39’ 230 kV line / single contingency (‘220-43’) loss of Linwood – Chichester ‘220-43’ 230 kV line and Phillips island generating units CT2, CT3, and ST
- Recommended Solution: Replace terminal equipment at Chichester
- Estimated Cost: \$0.475 M
- Expected In-Service: May 27, 2011

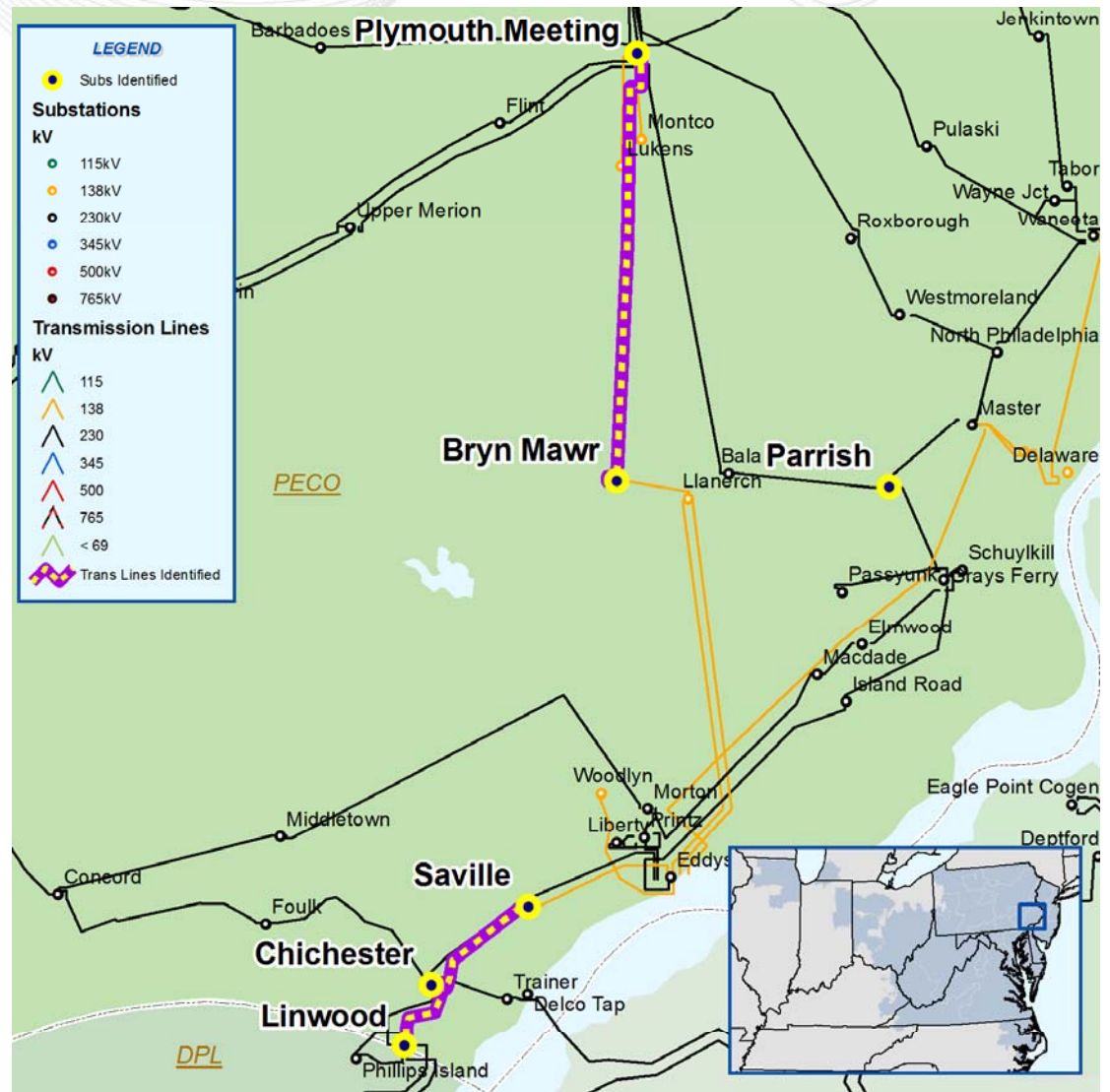




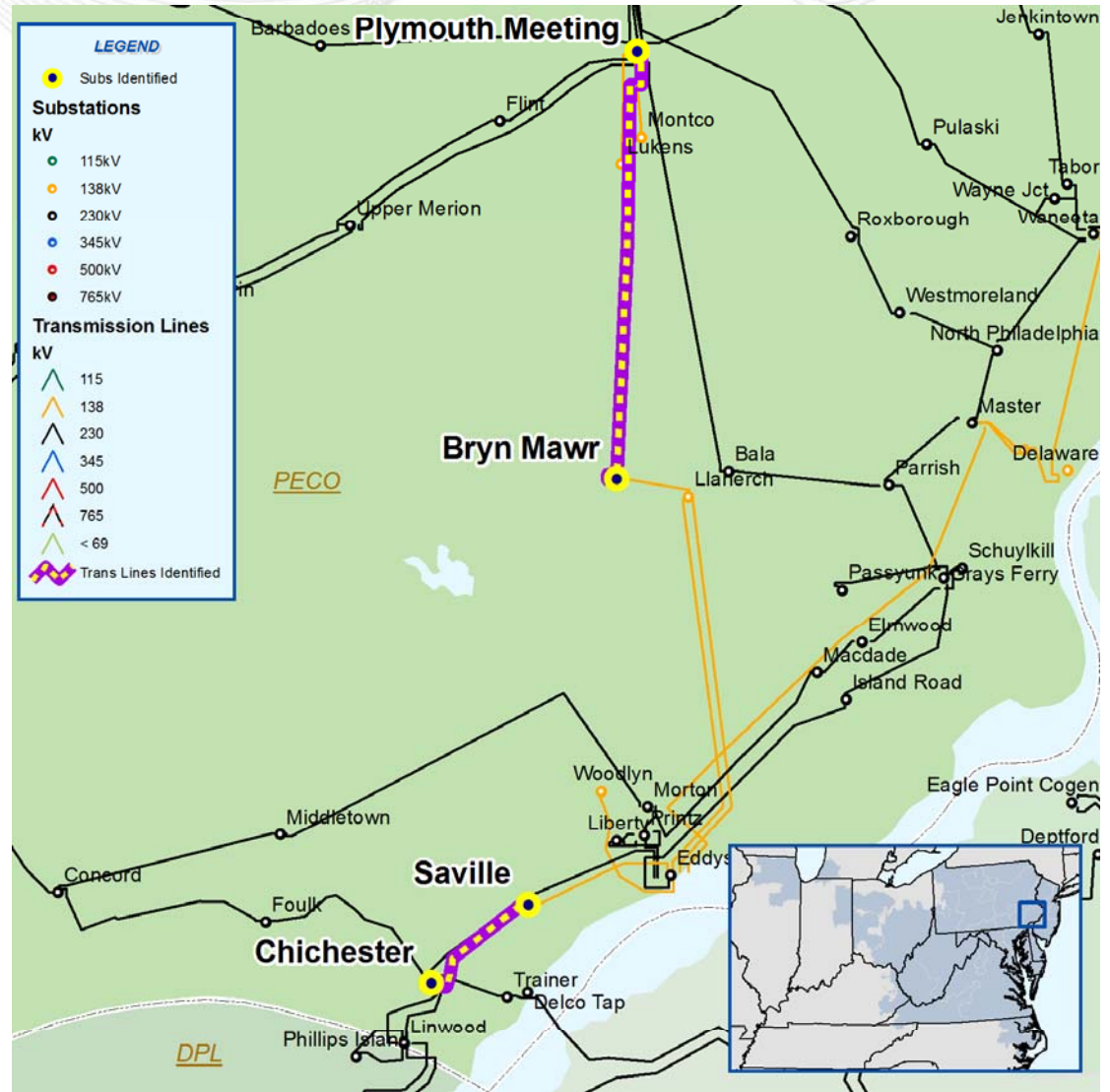
- Chichester – Saville 138 kV line overloaded for the following contingencies:
  - line fault with stuck breaker contingency ('GRAYS275') loss of Grays Ferry – Tunnel 230 kV line due to Grays Ferry stuck breaker '275'
  - bus contingency ('PLYM138B') loss of Plymouth Meeting 138 kV bus
  - single contingency ('220-27B') loss of Gays Ferry – Tunnel 230 kV line
  - Basecase for gen deliv test
  - loss of Macdade – Ridley – Morton 230 kV line (220-46) + loss of Island Road – Eddystone 230 kV line (220-23)
- Recommended Solution: Reconductor the line and upgrade terminal equipment
- Estimated cost: \$ 8.5 M
- Expected in-service: December 31, 2012



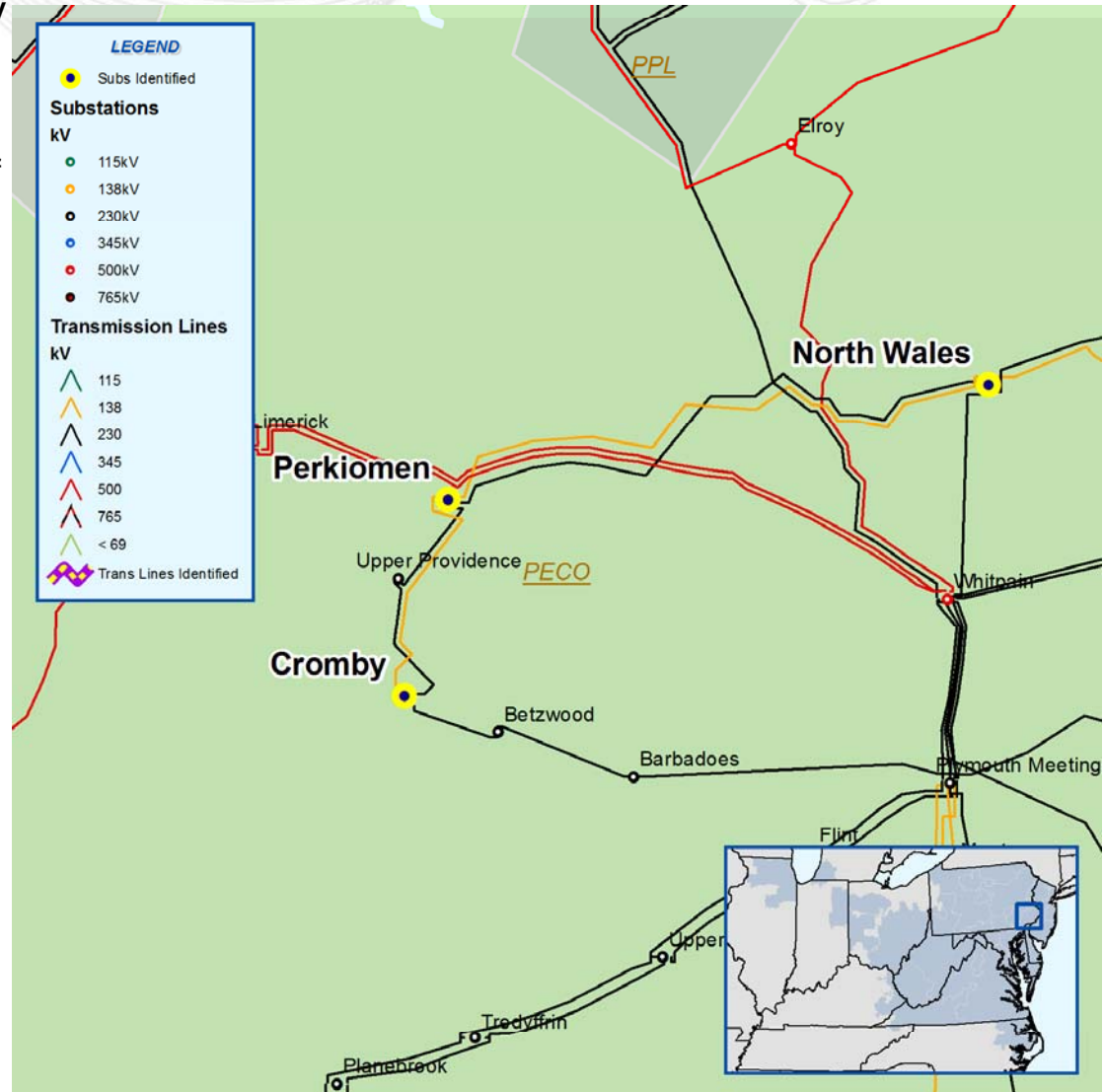
- Tunnel – Parrish 230 kV line overloaded for the following contingencies
  - single contingency ('PJM89\_A') loss of New Freedom – East Windsor 500 kV for gen deliv test
  - Basecase for gen deliv test
- Recommended Solution: Replace terminal equipment at Parrish
- Estimated Cost: \$0.15 M
- Expected In-Service: May 27, 2011



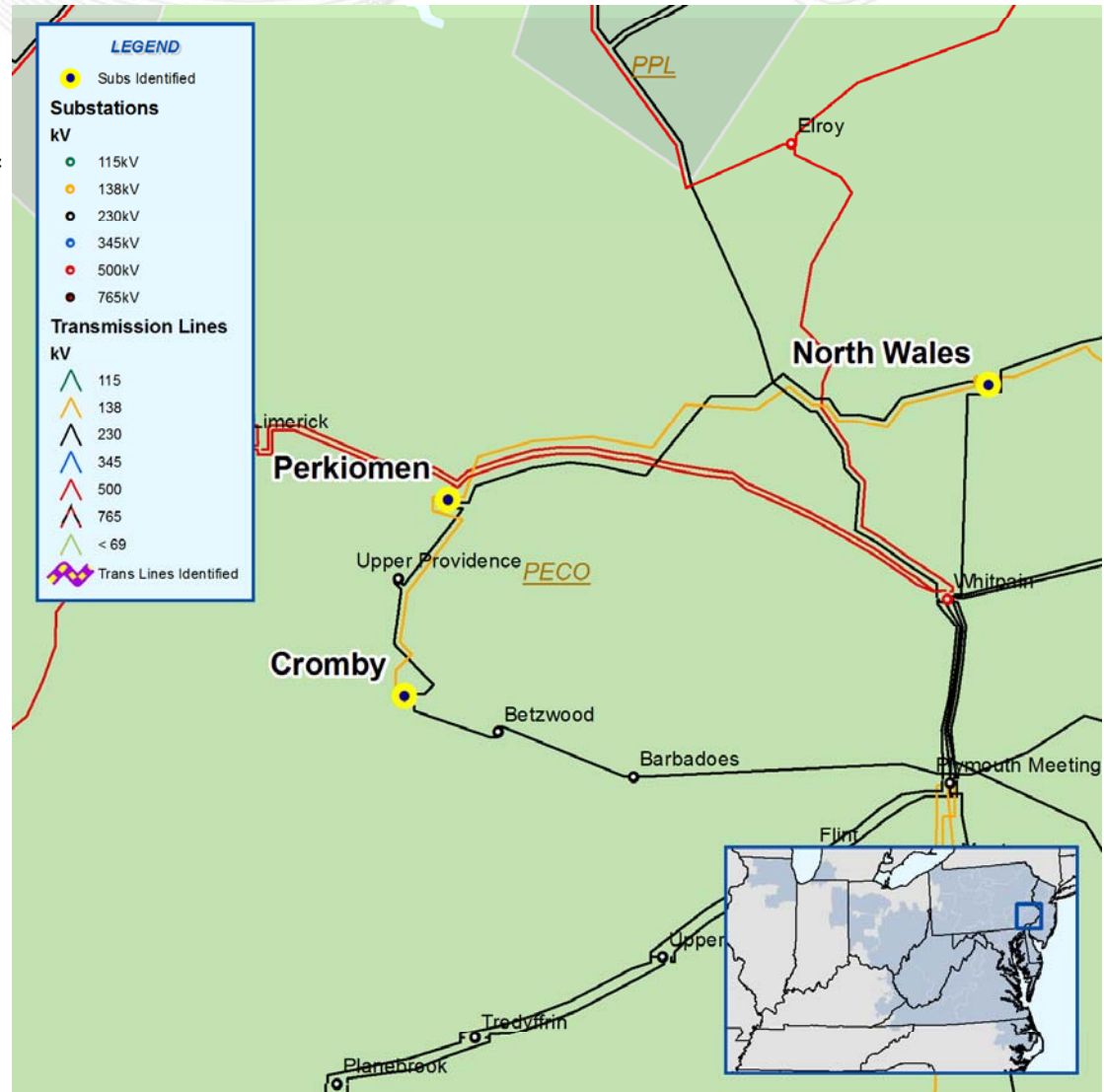
- Plymouth Meeting – Bryn Mawr 138 kV line overload for the following contingencies:
  - bus contingency ('CHI230B1') loss of Chichester bus section 1
  - line fault with stuck breaker contingency ('CHICH045') loss of Chichester – Foulk 230 kV line and Foulk 230/13.8 kV transformer #2 as well as Chichester bus section 1 due to the Chichester stuck breaker '045'
  - loss of Chichester 230/138 kV transformer (CHICH-T9) + Basecase
  - loss of Chichester 230/138 kV transformer (CHICH-T9) + Eddystone – Master 138 kV line (130-43)
  - line fault with stuck breaker contingency ('CHICH785') loss of the Chichester 230/138 kV transformer and Chichester 138/69 kV transformer s #7 & 8
- Recommended solution: Install 230/138 kV transformer at Eddystone
- Estimated cost: \$3.6 M
- Expected in-service: June 1, 2011



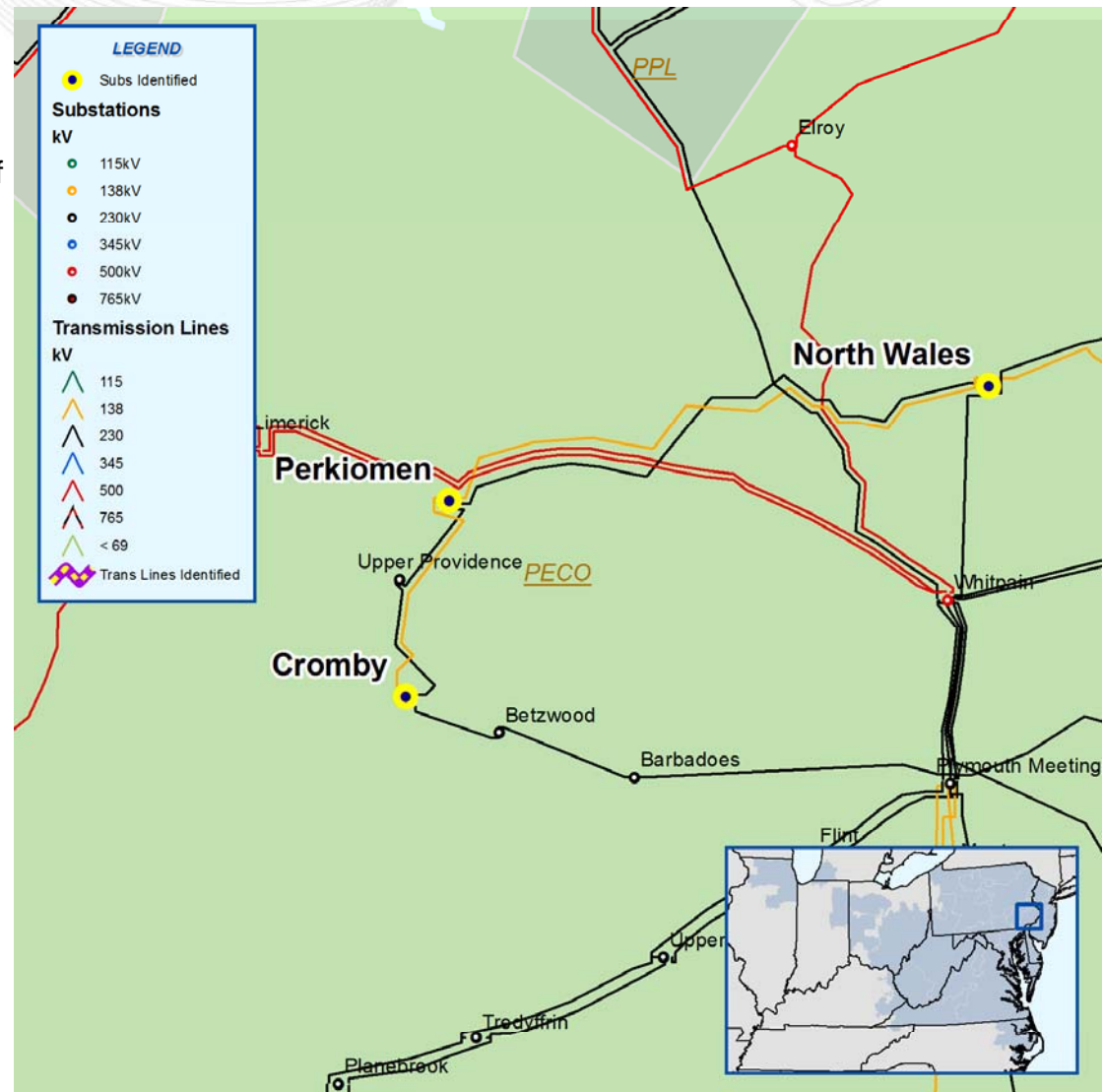
- North Wales and Heaton 138 kV area low voltage violations for the following contingencies
  - bus contingency ('HEAT138B') loss of Heaton 138 kV station bus section 2
  - line fault with stuck breaker contingency ('HEAT0805') loss of Heaton – Woodbourne 230 kV line with stuck breaker 805
  - line fault with stuck breaker contingency ('HEAT0995') loss of Heaton – Woodbourne 230 kV line with stuck breaker 995
- Recommended Solution: Add a second 230/138 kV transformer at Heaton. Add a circuit breaker on the Heaton – North Wales 138 kV line. Add a 35 MVAR capacitor at Heaton
- Estimated cost: \$7.754 M
- Expected in-service: December 16, 2011



- Cromby 138 kV station low voltage violations for the following contingencies:
  - bus contingency ('HEAT138B') loss of Heaton 138 kV station bus section 2
  - line fault with stuck breaker contingency ('HEAT0805') loss of Heaton – Woodbourne 230 kV line with stuck breaker 805
  - line fault with stuck breaker contingency ('HEAT0995') loss of Heaton – Woodbourne 230 kV line with stuck breaker 995
- Recommended Solution: Replace 230/69 kV transformer #6 at Cromby. Add two 50 MVAR 230 kV capacitor banks at Cromby
- Estimated Cost: \$ 6.142 M
- Projected in-service: December 31, 2011



- Perkiomen 138 kV station voltage violations for the following contingencies:
  - bus contingency ('HEAT138B') loss of Heaton 138 kV station bus section 2
  - line fault with stuck breaker contingency ('HEAT0805') loss of Heaton – Woodbourne 230 kV line with stuck breaker 805
  - line fault with stuck breaker contingency ('HEAT0995') loss of Heaton – Woodbourne 230 kV line with stuck breaker 995
- Recommended Solution: Add 138 kV circuit breakers at Cromby, Perkiomen, and North Wales. Add a 35 MVAR 138 kV capacitor at Perkiomen
- Estimated Cost: \$ 3.9 M
- Expected In-Service: August 1, 2011



- Eddystone 230 kV CB #365
  - Recommended solution: Upgrade the circuit breaker
  - Estimated Cost: \$0.125 M
  - Expected In-Service: May 31, 2011
  
- Eddystone 230 kV CB #785
  - Recommended solution: Upgrade the circuit breaker
  - Estimated Cost: \$0.125 M
  - Expected In-Service: May 31, 2011

- Eddystone 230 kV CB #35
  - Recommended solution: Upgrade / replace the circuit breaker
  - Estimated Cost: TBD
  - Expected In-Service: May 27, 2011
- Eddystone 230 kV CB #45
  - Recommended solution: Upgrade the circuit breaker
  - Estimated Cost: TBD
  - Expected In-Service: May 27, 2011
- Note: Both of these circuit breakers are Exelon Power circuit breakers



- As noted on the previous slides a number of upgrades are not expected to be placed in-service until after the requested deactivation date
- PJM notified Exelon Power that Cromby #2 is needed for reliability until December 31, 2011 and Eddystone #2 is needed for reliability until December 31, 2012

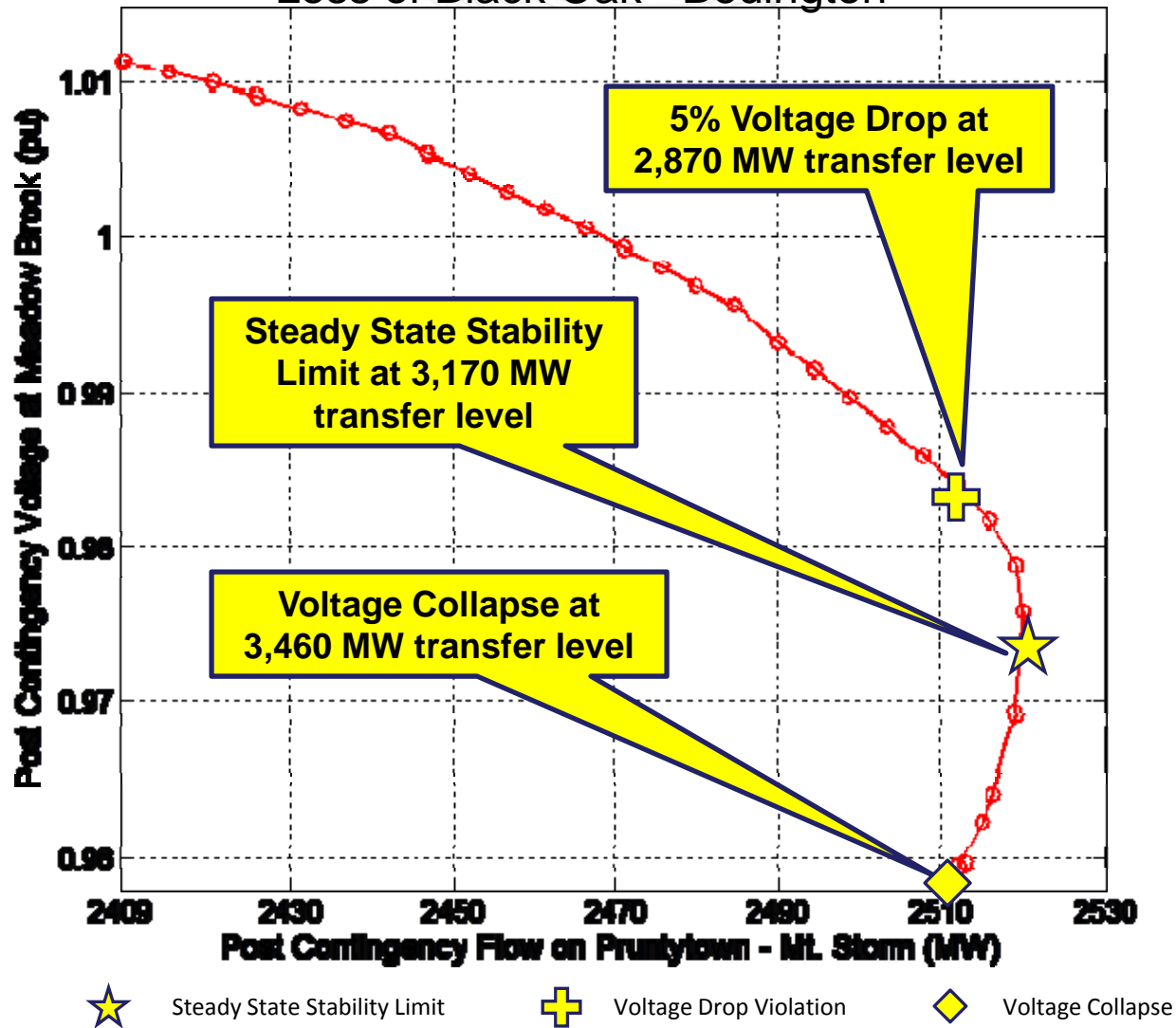


# Baseline Reliability Update – Potential Reliability Violations

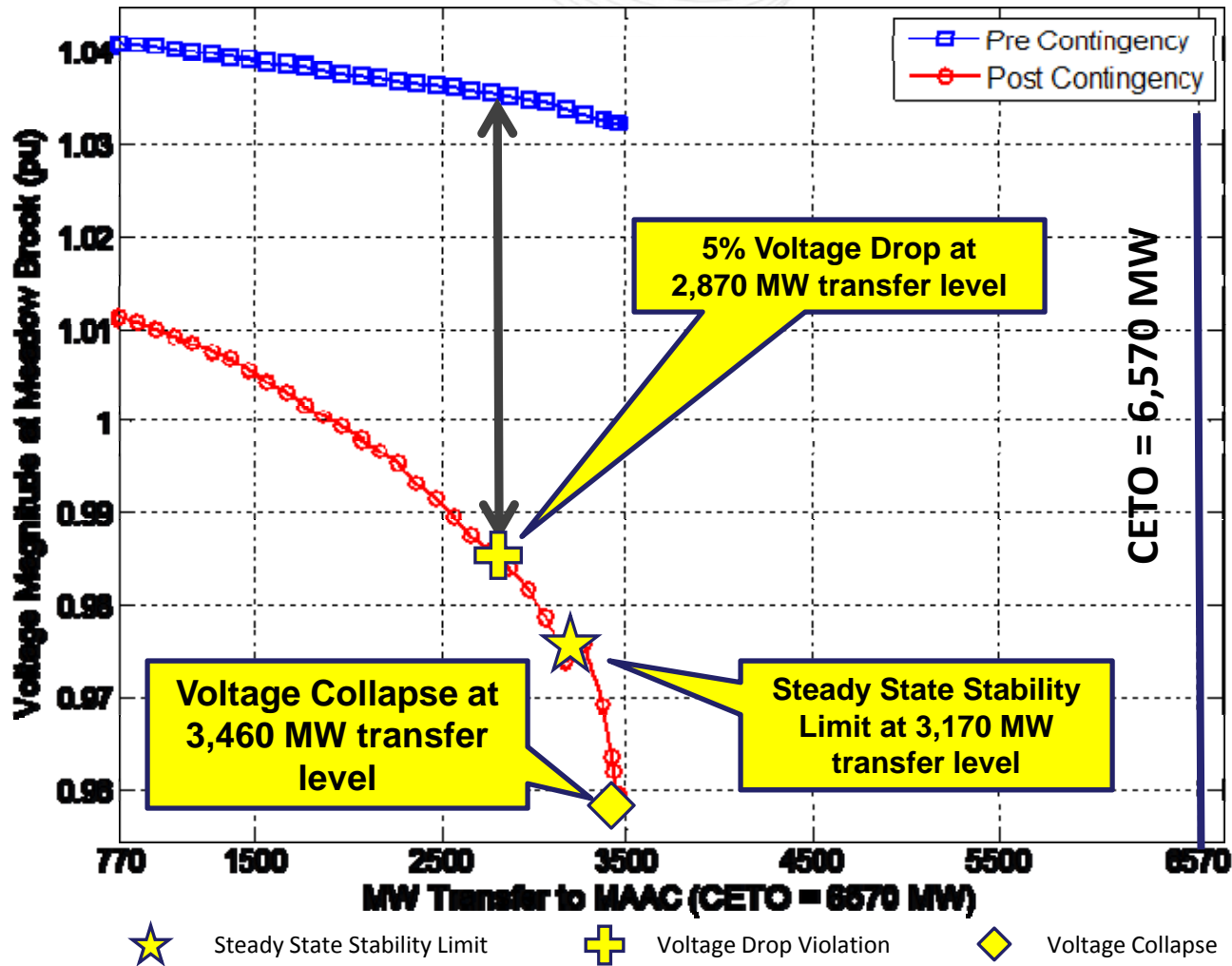
- 2015 Load Deliverability Voltage and Load Deliverability Thermal Testing
  - Several areas have passed with no Potential reliability violations
    - AEP
    - Atlantic Electric
    - DPL
    - DPL South
    - Duquesne
    - Meted
    - Penelec
    - PECO
    - PPL
    - WMAAC
- 2015 Generator Deliverability and 2015 N-1-1 Thermal underway for all areas
- 2015 N-1-1 thermal is in-progress. Voltage will begin following the thermal testing.

- **Several critical contingencies are non-covergent**
  - Keystone - South Bend 500 kV
  - Conemaugh - Keystone 500 kV
  - Conemaugh - Jacks Mountain 500 kV
  - Keystone - Jacks Mountain 500 kV
  - Jacks Mountain - Juniata 1&2 500 kV
  - Conemaugh - Hunterstown 500 kV
  - Hunterstown - Conastone 500 kV
  - Conastone - Brighton 500 kV
  - Brighton - Doubs 500 kV
  - Calvert Cliffs - Waugh Chapel 500 kV
  - Burches Hill - Possum Point 500 kV
  - Brister - Ox 500 kV
  - Elmont - Cunningham 500 kV
  - Elmont - Ladysmith 500 kV
  - Ladysmith - Possum Point 500 kV
  - Loudoun - Morrisville 500 kV
  - Morrisville - North Anna 500 kV
  - Loudoun - Pleasant View 500 kV
  - Meadow Brook - Loudoun 500 kV
  - Mount storm - Meadow Brook 500 kV
  - Mount Storm - Greenland Gap 500 kV
  - Mount Storm - T157 Tap 500 kV
  - T157 Tap - Doubs 500 kV
  - Hatfield - Black Oak 500 kV
  - Hatfield - Ronco 500 kV
  - Hatfield - Banyan Run 500 kV
  - Bedington - Black Oak 500 kV
  - Bedington - Doubs 500 kV
  - Fort Martin - Ronco 500 kV
  - Yukon - South Bend 500 kV
  - Yukon - Banyan Run 500 kV
  - Cabot - Cranberry 500 kV
  - Cranberry - Wylie Ridge 500 kV
  - Calvert Cliffs 1&2 500 kV
  - P04 500 kV
  - Susquehanna #2

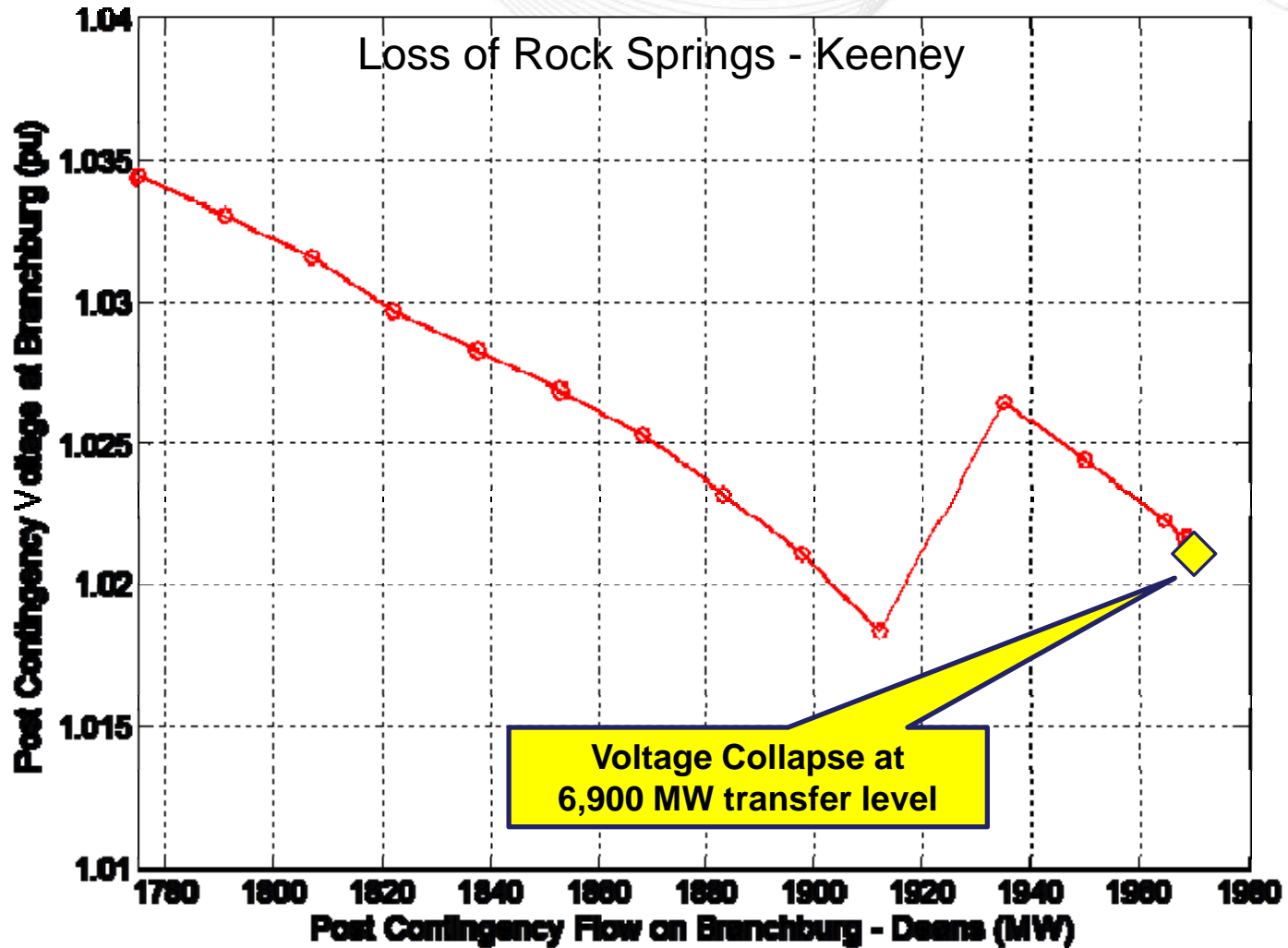
## Loss of Black Oak - Bedington



## Loss of Black Oak - Bedington



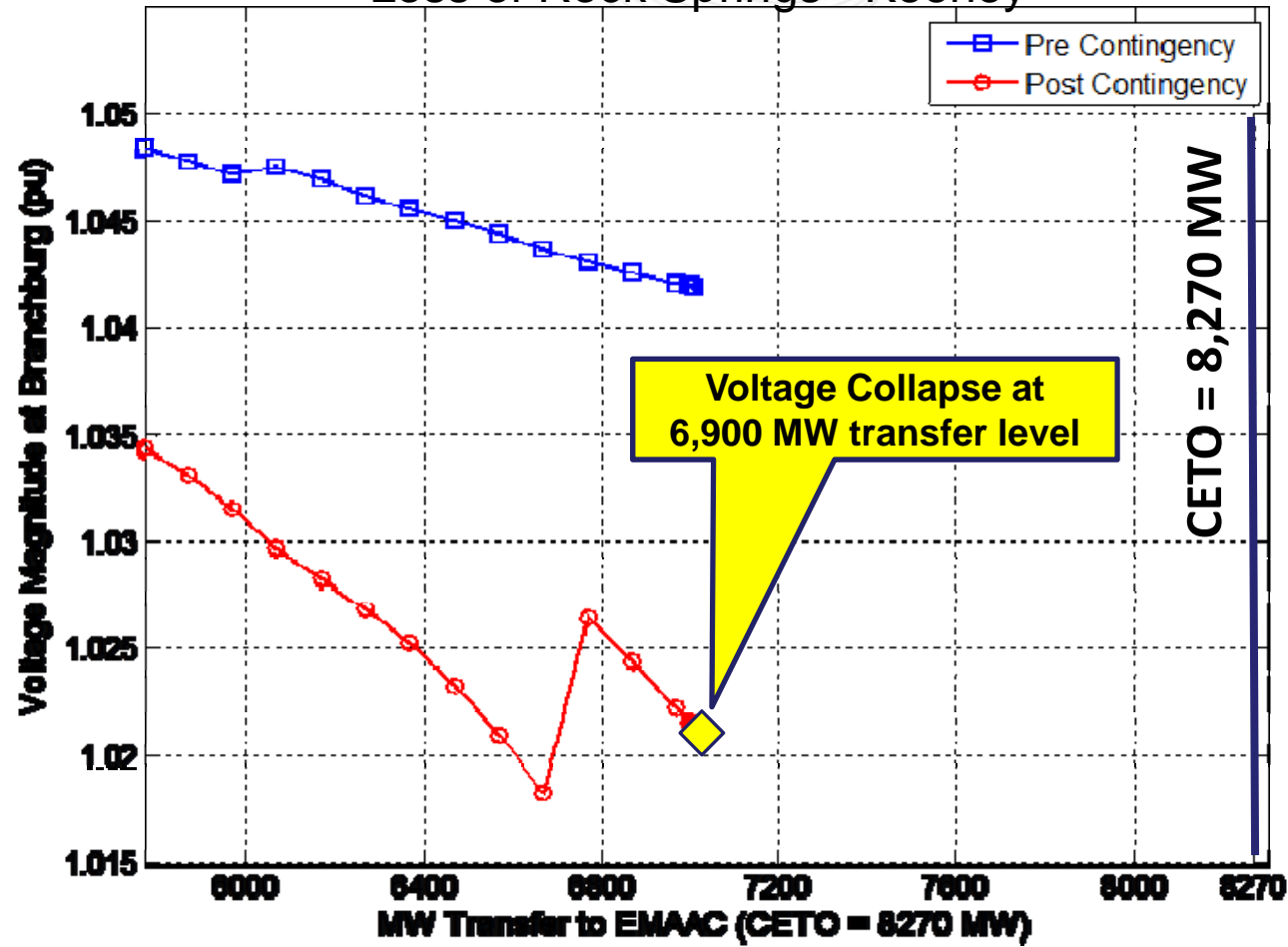
- Several critical contingencies are non-convergent
  - Red Lion to Hope Creek 500 kV
  - New Freedom to East Windsor 500 kV
  - Conemaugh to Hunterstown 500 kV
  - Hunterstown to Conastone 500 kV
  - Susquehanna to Lackawanna 500 kV
  - Lackawanna to Hopatcong 500 kV
  - Hopatcong to Roseland 500 kV
  - Keeney to Rock Springs 500 kV
  - Rock Springs to Peach Bottom 500 kV
  - Peach Bottom to Limerick 500 kV
  - Alburtis to Branchburg 500 kV
  - Smithburg to Deans 500 kV
  - Keystone to Jacks Mt. 500 kV
  - Branchburg to Elroy 500 kV
  - Ford Mill 600 MW generator
  - Ford Mill 600 MW generator
  - Branchburg 400 MVAR capacitor
  - Bergen 550 MW generator
  - Linden 750 MW generator



- ★ Steady State Stability Limit
- ✚ Voltage Drop Violation
- ◆ Voltage Collapse

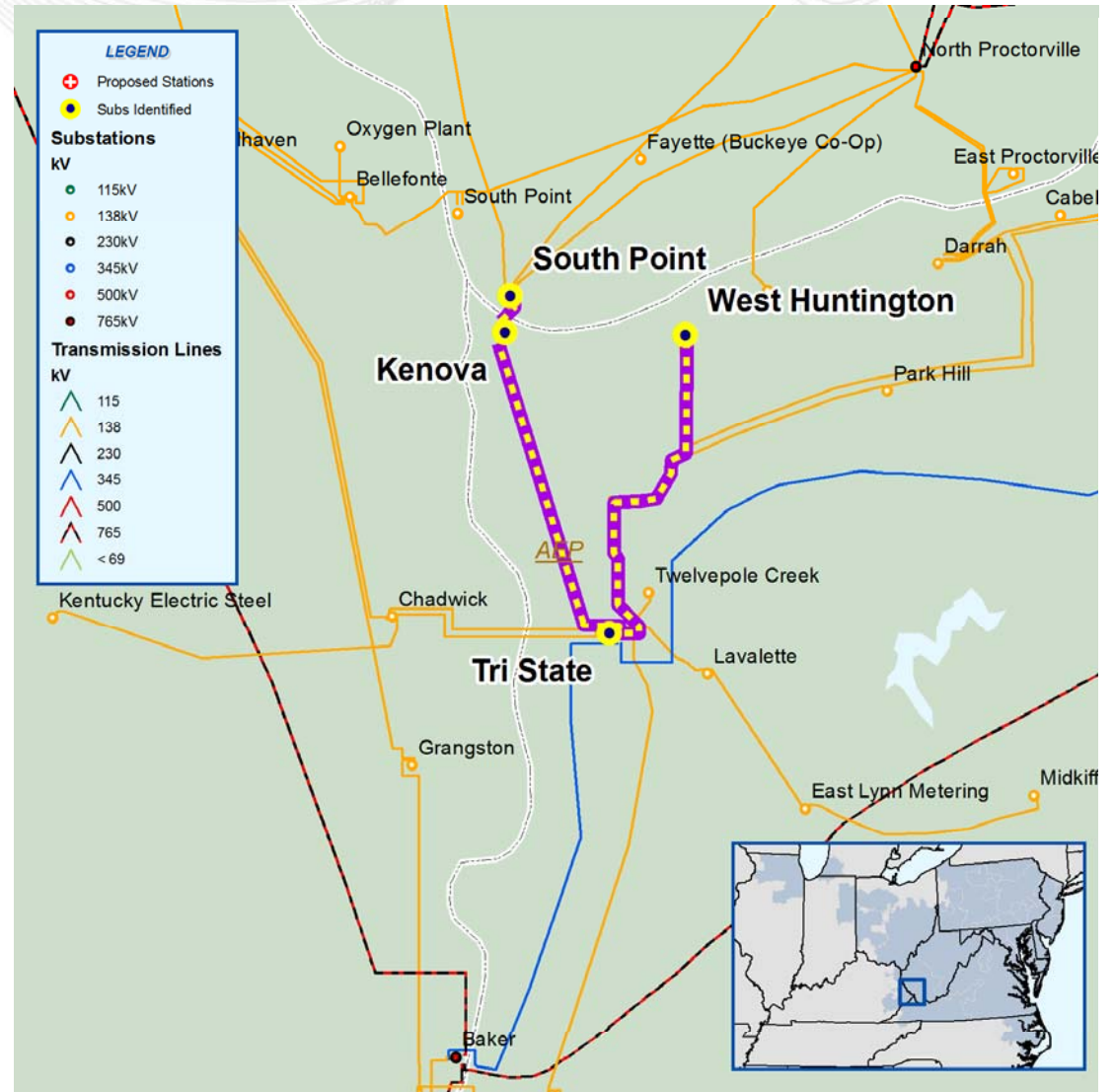


## Loss of Rock Springs - Keeney



- ★ Steady State Stability Limit
- + Voltage Drop Violation
- ◇ Voltage Collapse

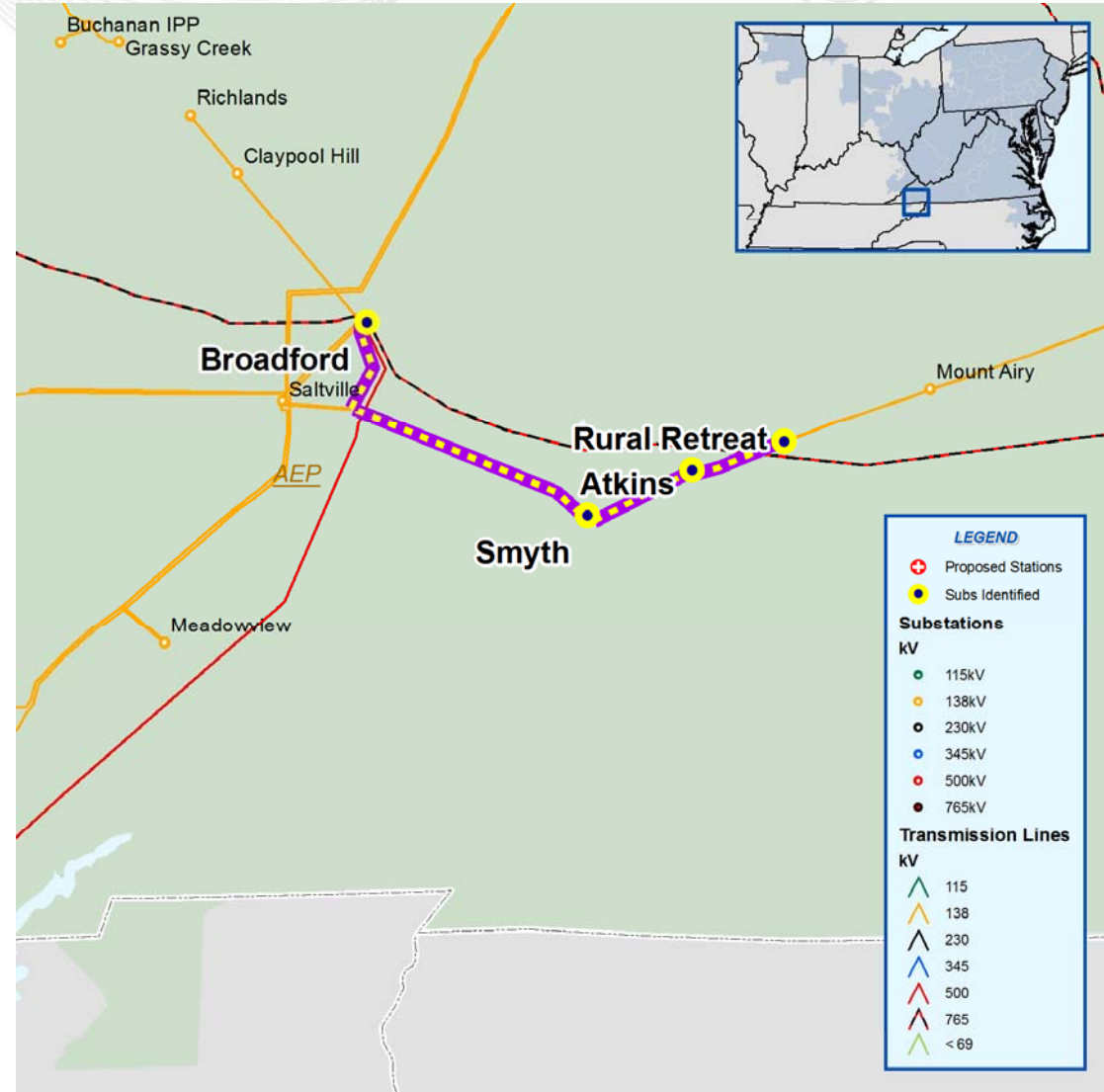
- Potential generator deliverability violations
- Tristate – Kenova 138 kV line overload for the loss of the Baker 765/345 kV transformer
- Kenova – South Point 138 kV line overload for the loss of the Baker 765/345 kV transformer
- Tristate – West Huntington 138 kV line overload the loss of the Baker 765/345 kV transformer





## AEP Transmission Zone

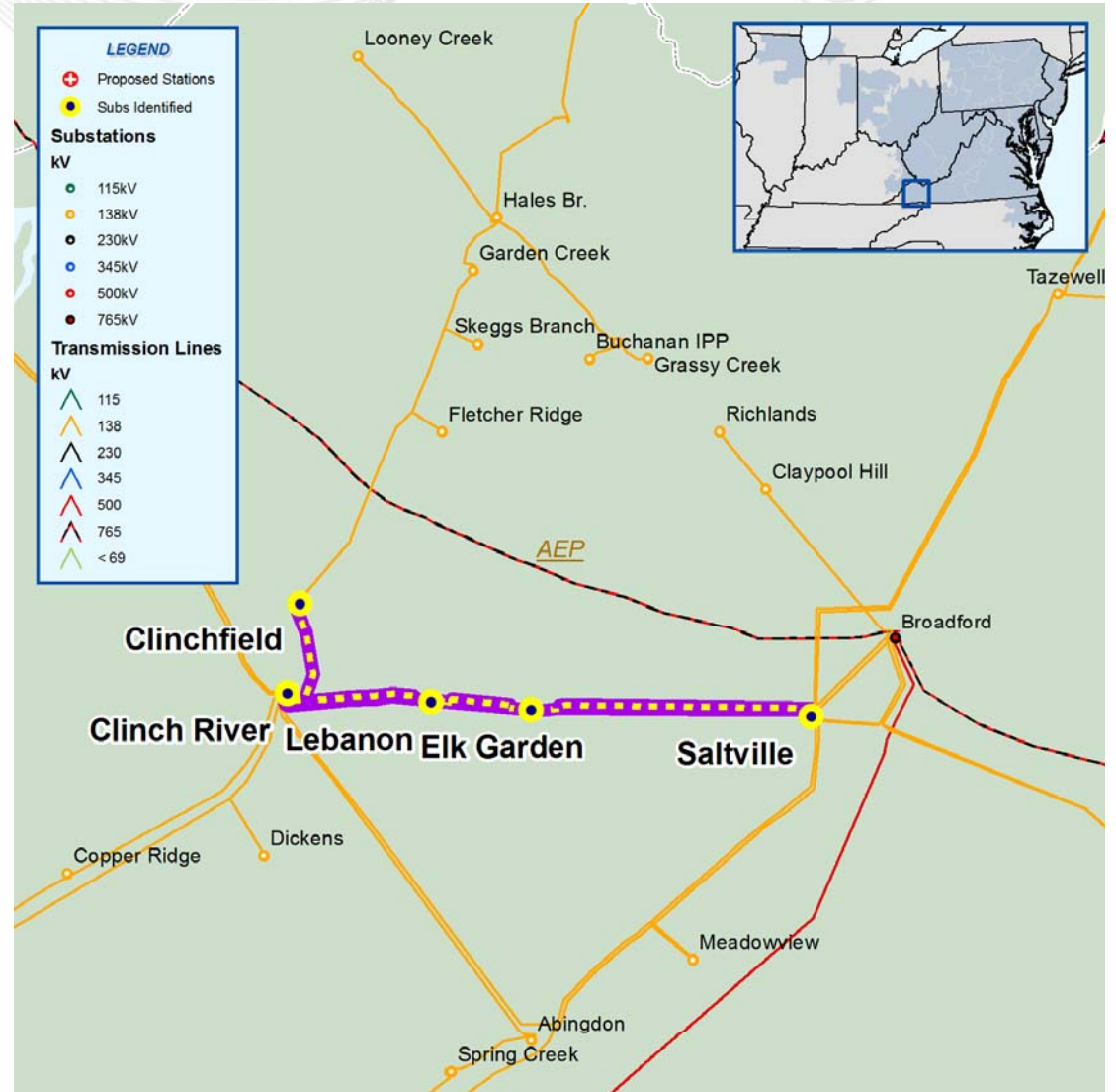
- Potential common mode outage violations
- Broadford - Smyth 138 kV line overload for the stuck breaker contingency with the loss of the Jackson Ferry – Cloverdale 765 kV line and Jackson Ferry 765/138 kV transformer #2, or for the stuck breaker contingency with the loss of the Jackson Ferry – Broadford 765 kV line and Jackson Ferry 765/138 kV transformer #2
- Smyth - Atkins 138 kV line overload for the stuck breaker contingency with the loss of the Jackson Ferry – Cloverdale 765 kV line and Jackson Ferry 765/138 kV transformer #2
- Atkins– Rural Retreat 138 kV line overload for the stuck breaker contingency with the loss of the Jackson Ferry – Cloverdale 765 kV line and Jackson Ferry 765/138 kV transformer #2



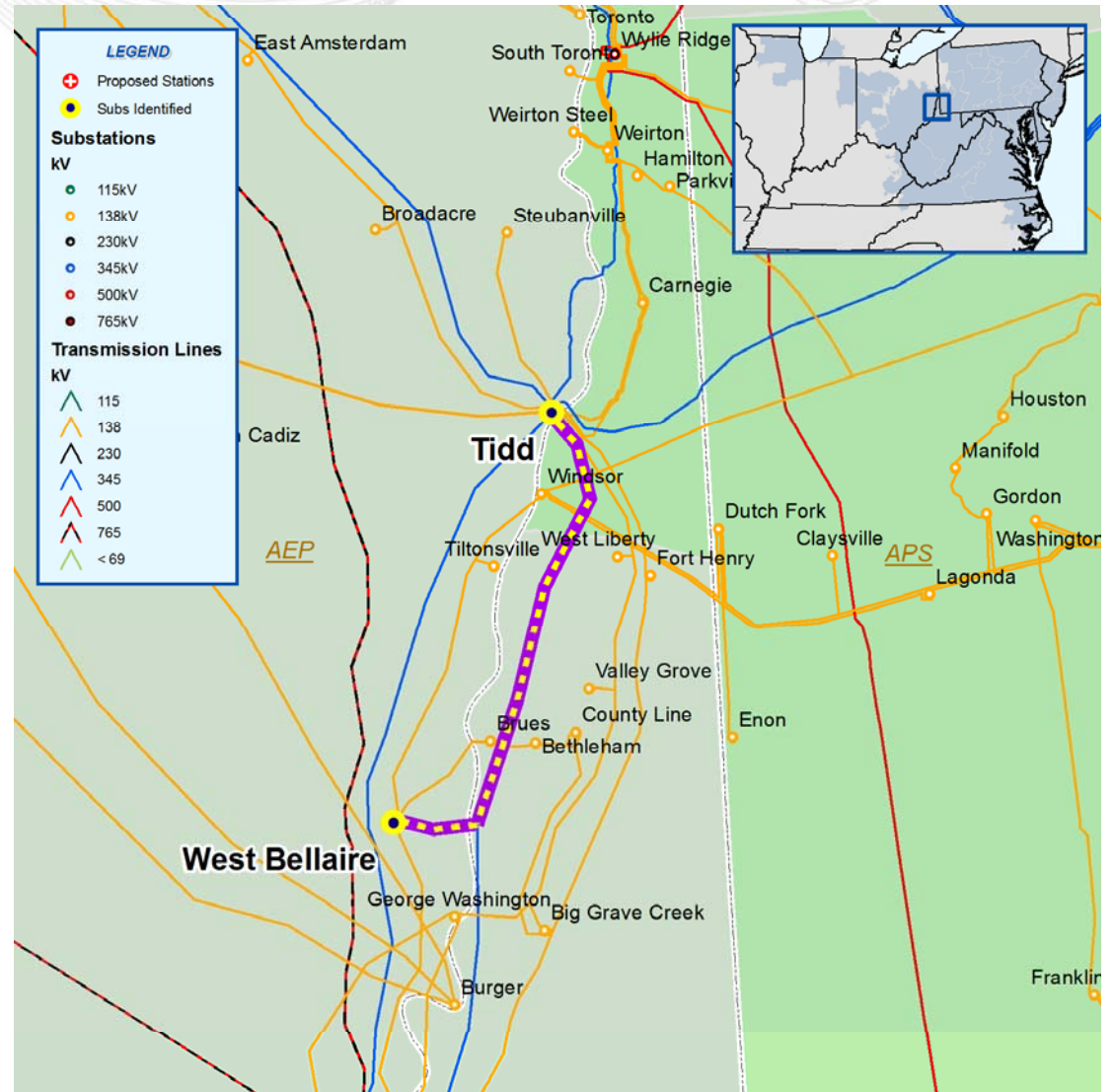
- Potential common mode outage violations
- Otter – Johnson Mountain – New - London 138 kV line overload for several contingencies



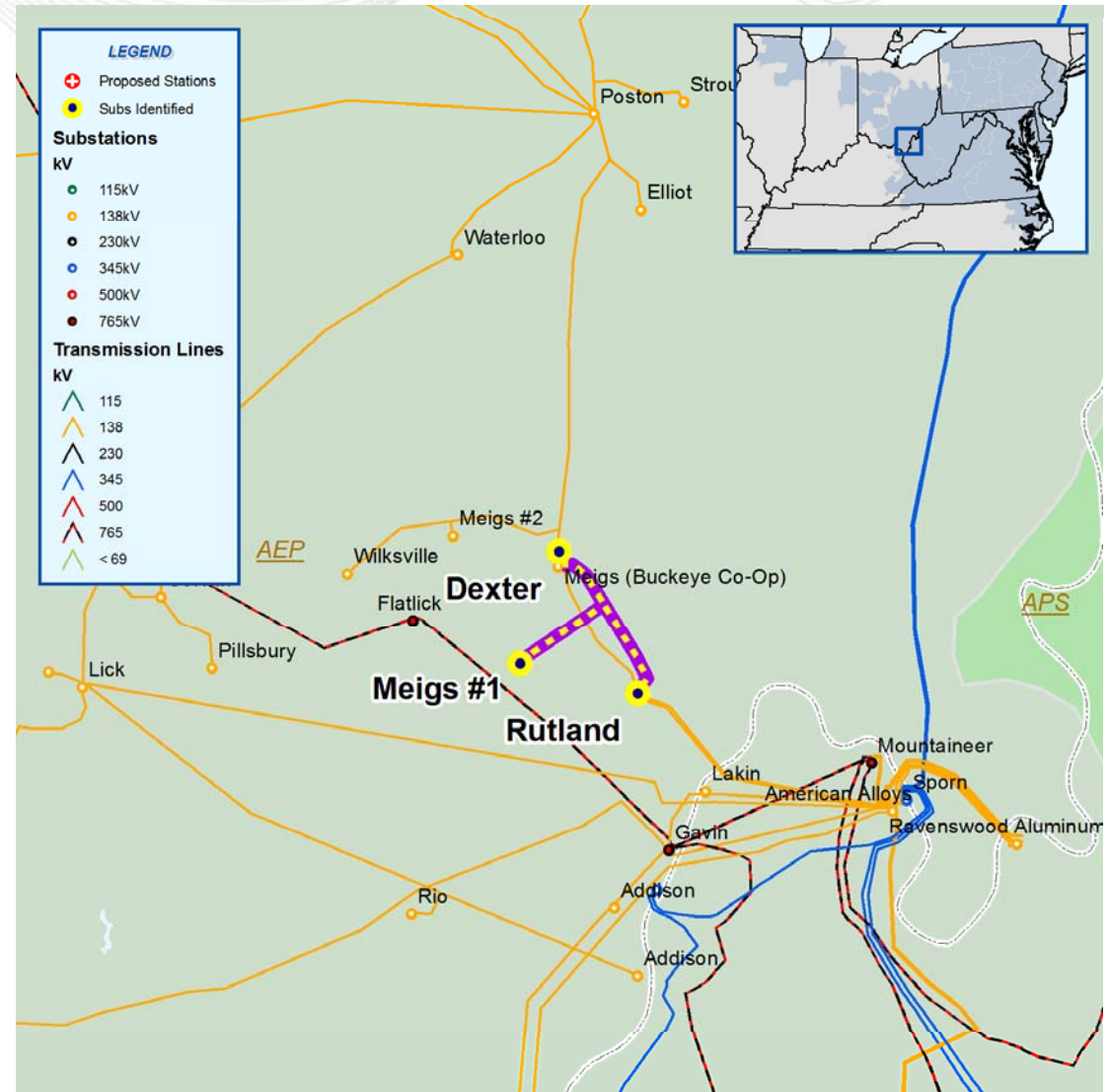
- Potential common mode outage violations
- Wolf Hill – North Bristol 138 kV line overload for several contingencies
- Elk Garden - Saltville 138 kV line overload for several contingencies
- Clinch River - Lebanon 138 kV line overload for several contingencies
- Clinch River - Clinchfield 138 kV line overload for the loss of the Clinch River – Freemont 138 kV line



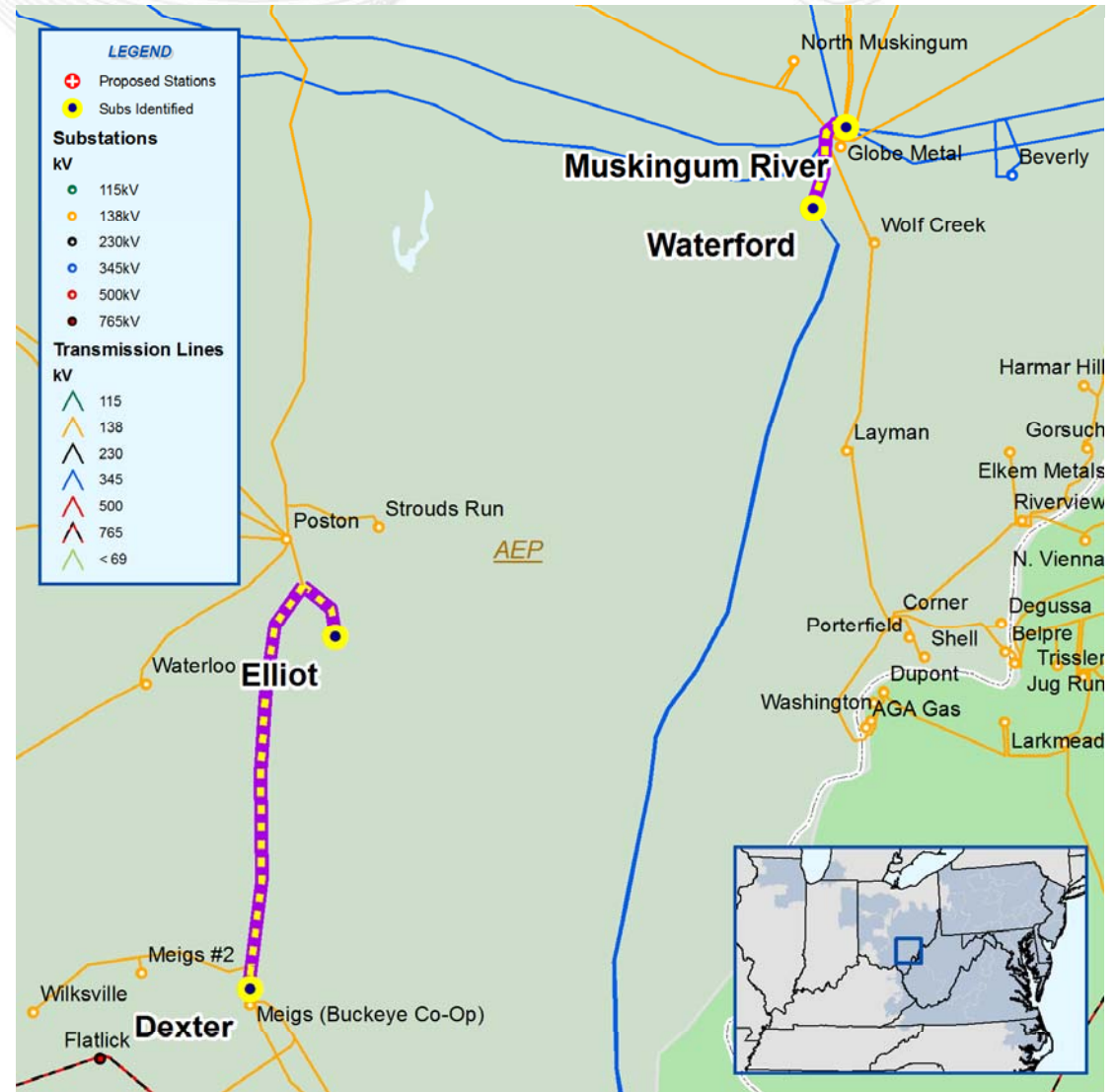
- Potential common mode outage violations
- West Bellaire – Tidd 345 kV line overload for the line with stuck breaker contingency with loss of Kammer – South Canton 765 kV line, Kammer 765/500 kV transformer, South Canton 765/345 transformer #3, 502 Junction – Kammer 500 kV line and the South Canton 345/138 kV transformer



- Potential common mode outage violations
- Rutland – Meigs Mine 138 kV line overload for the loss of Muskingum - Waterford 345 kV line or further loss Muskingum unit #2
- Meigs Mine - Dexter 138 kV line overload for the loss of Muskingum - Waterford 345 kV line or further loss Muskingum unit #2
- SOLIDA – Bellefonte 138 kV line overload for the loss of the North Proctorville – SOLIDA 138 kV line

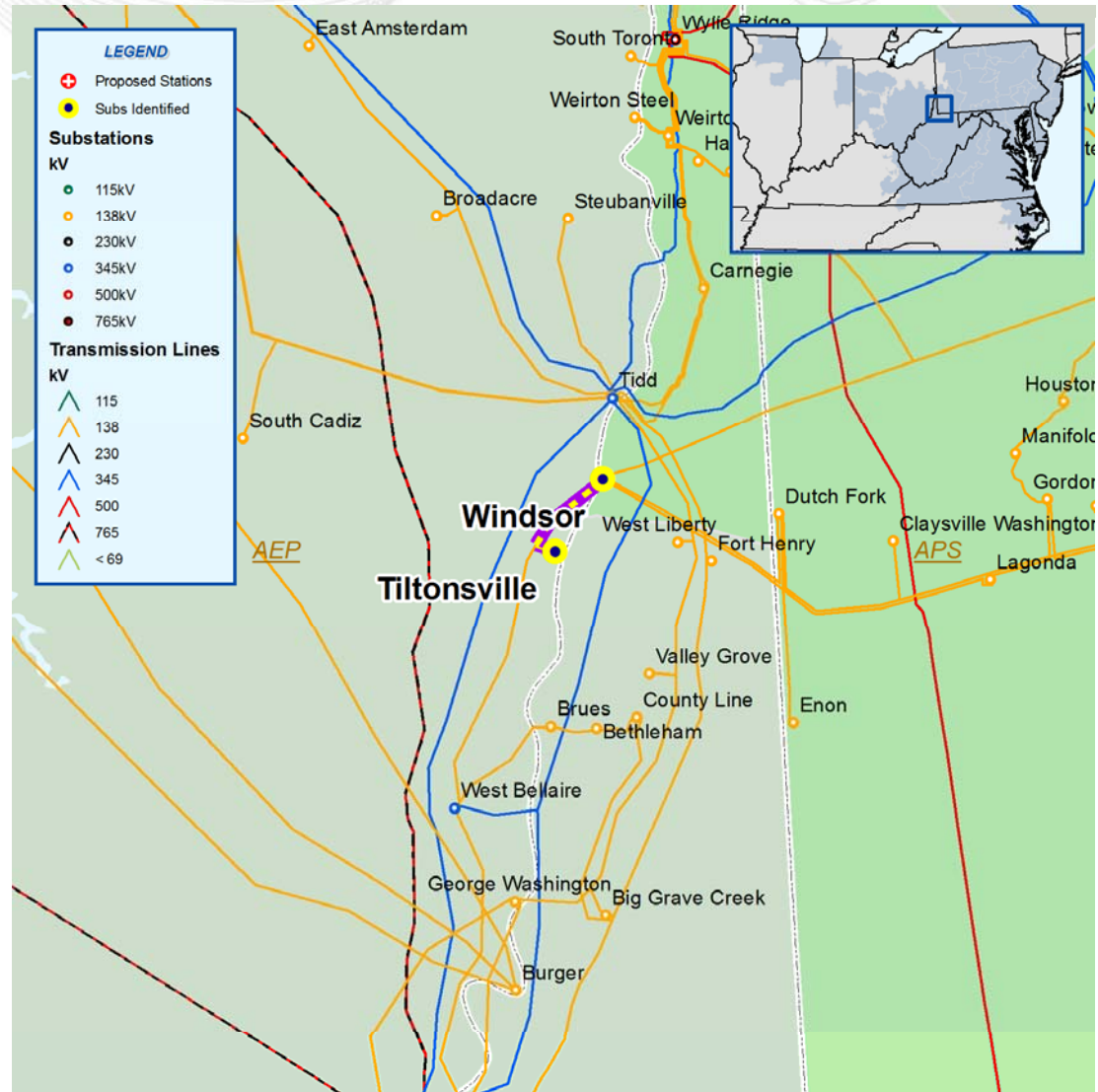


- Potential generator deliverability violations
- Dexter – Elliot 138 kV line overload for the loss of Muskingum – Waterford 345 kV line
- Waterford – Muskingum River 345 kV line overload for the non-contingency condition
- Muskingum River 345/138 kV transformer overload for several contingencies

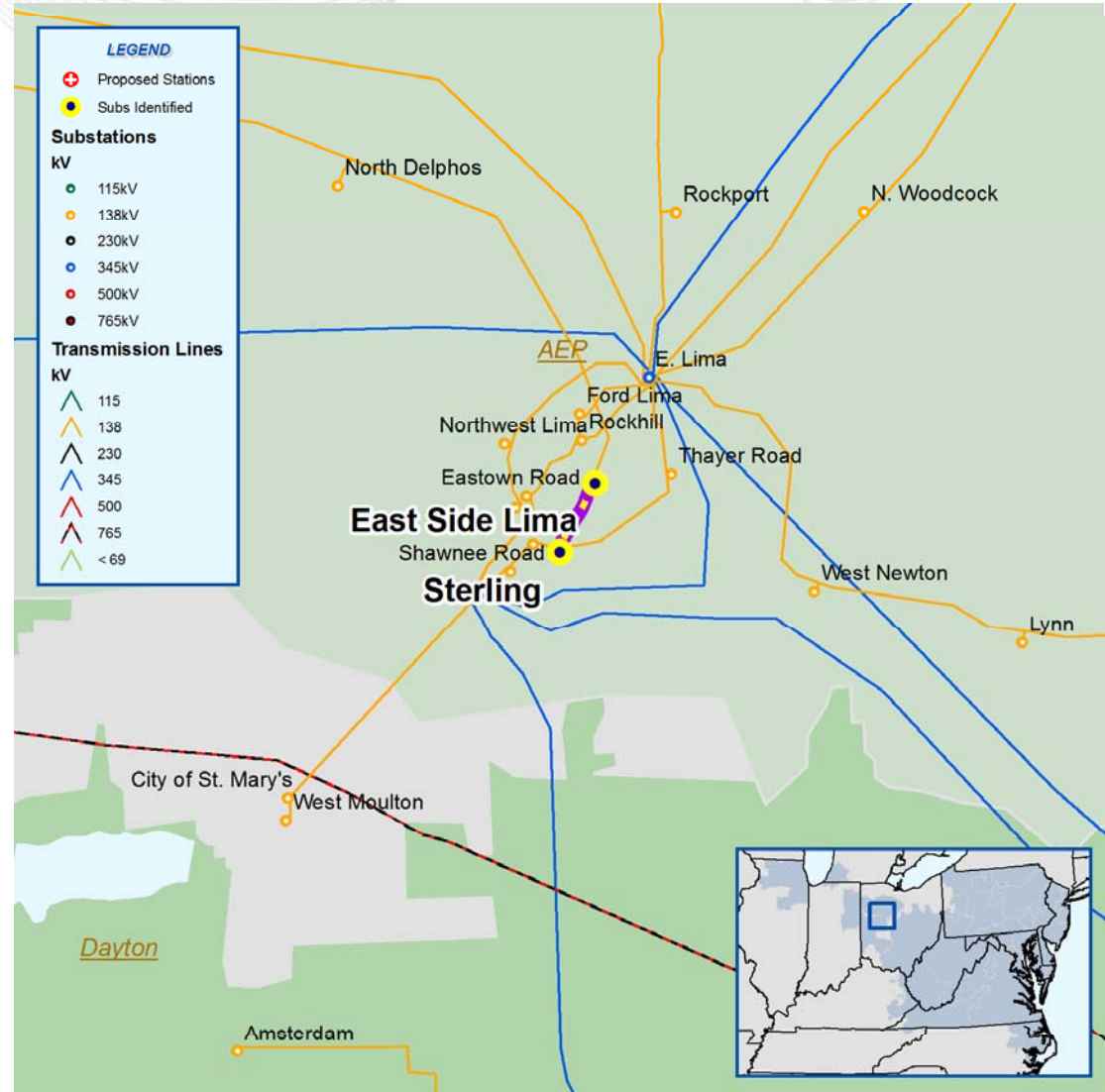




- Potential generator deliverability violations
- Tiltonsville – Windsor 138 kV line overload for several contingencies



- Potential generator deliverability violations
- Sterling – East Side 138 kV line overload for several contingencies



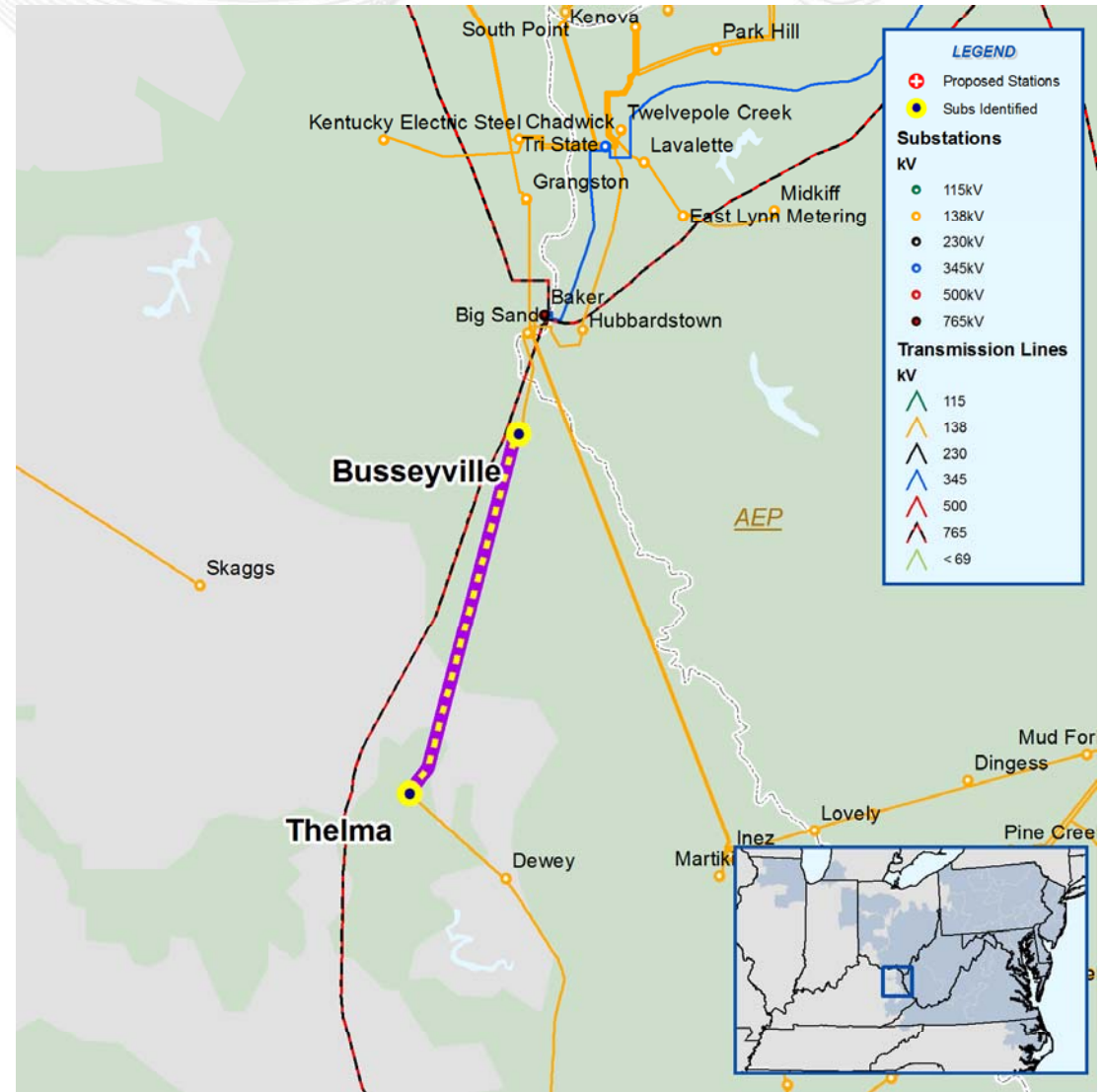
- Potential common mode outage violation
- Corner – Washington 138 kV line overload for the common tower outage of the Belmont – Trissler 138 kV line #1 and the Belmont – Edgelawn 138 kV line
- Ross – S Delano 138 kV line overload for several contingencies
- Circleville – Harrison 138 kV line overload for several contingencies
- Stroud Z – Stroud 138 kV line overload for the loss of the Dexter – Elliot - Poston 138 kV line



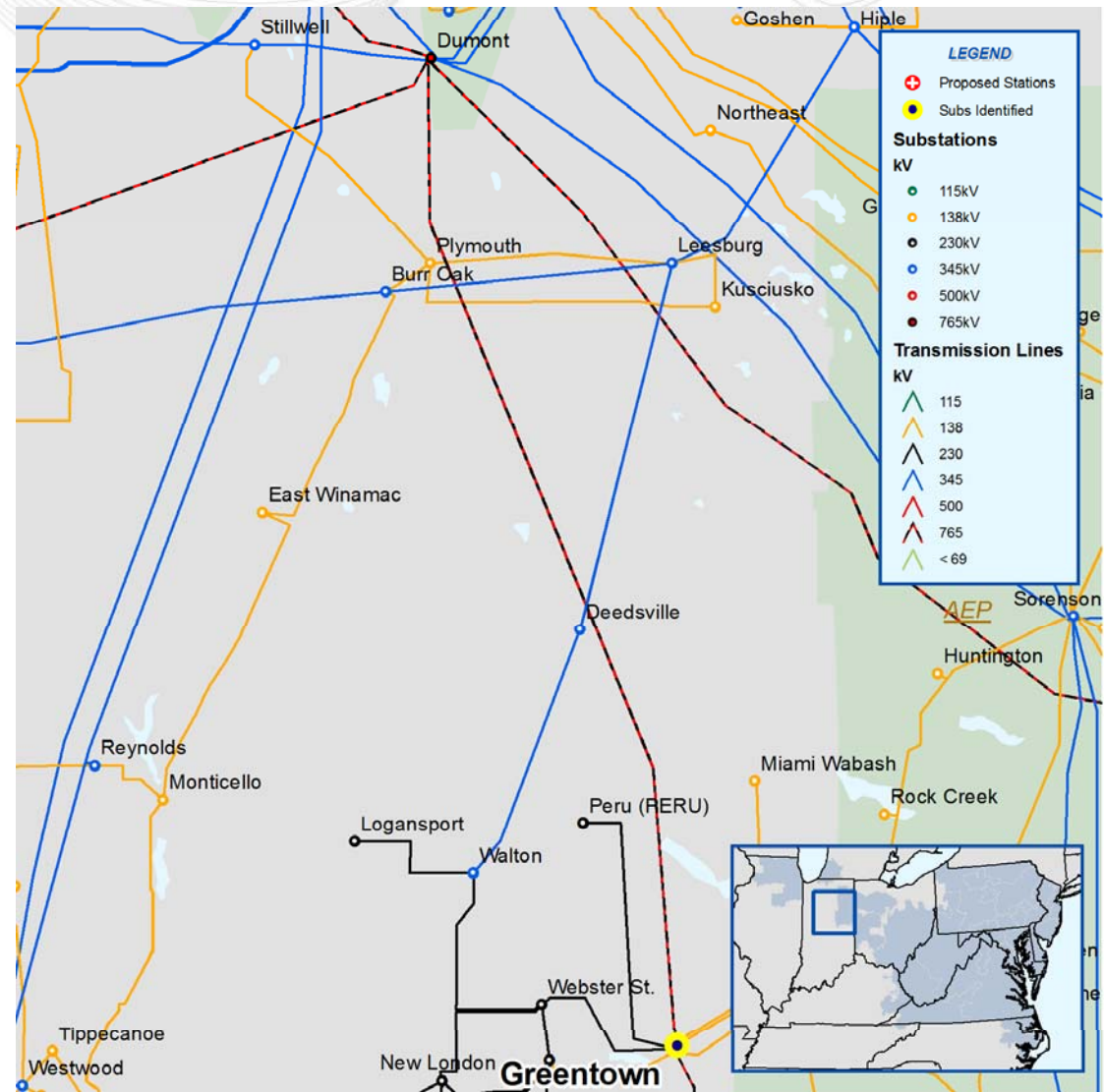
- Potential common mode outage violations
- S Delano - Delano 138 kV line overload for several contingencies
- Harris – Obetz 138 kV line overload for the line with stuck breaker contingency with the loss of Bixby – N Fork 345 kV line and Bixby 345/138 kV transformer #1 and #2



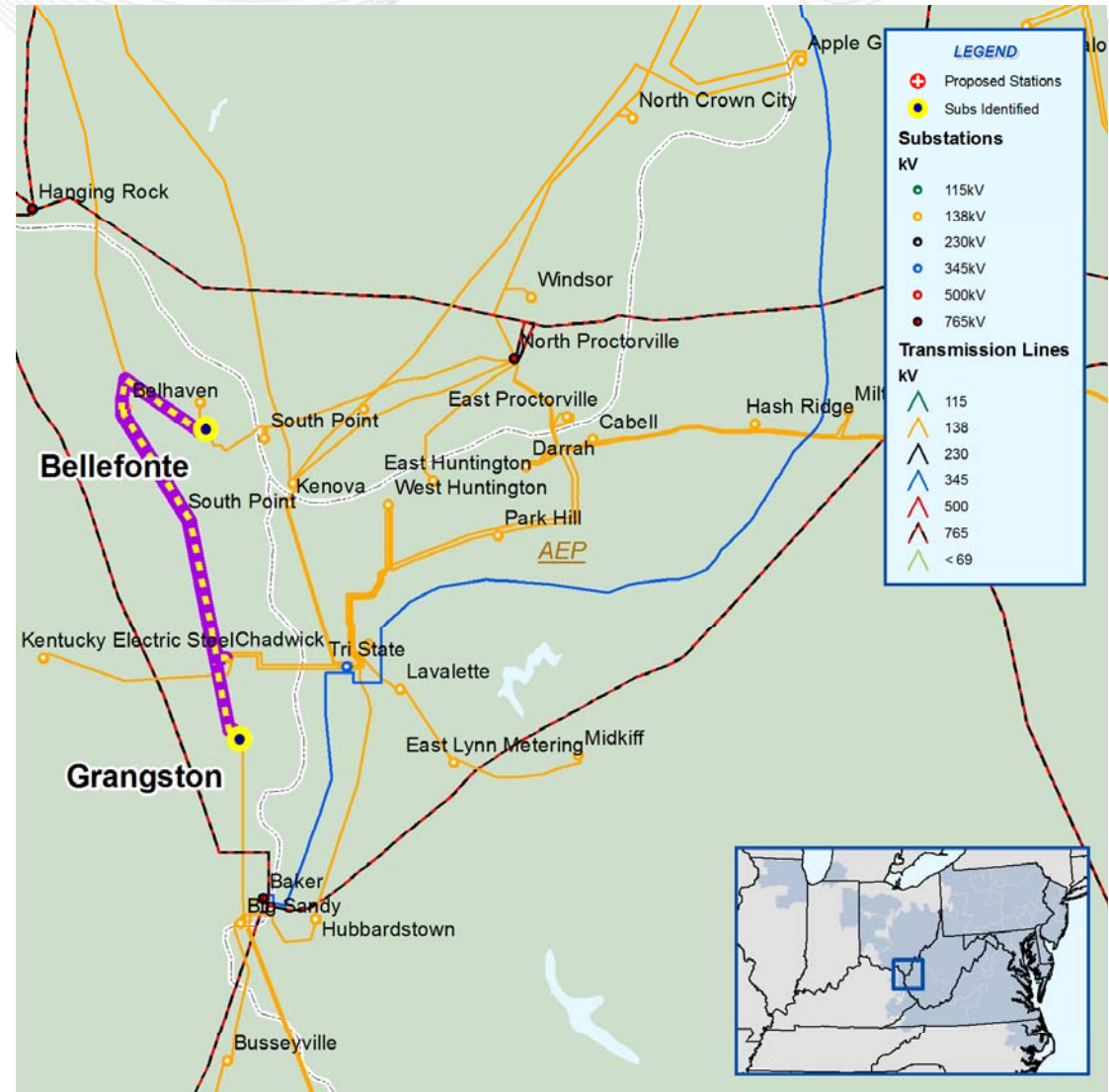
- Potential common mode outage violations
- Busseyville – Thelma 138 kV line overload for the line with stuck breaker contingency with the loss of Baker – Broadford 765 kV line and Baker 765/345 kV transformer



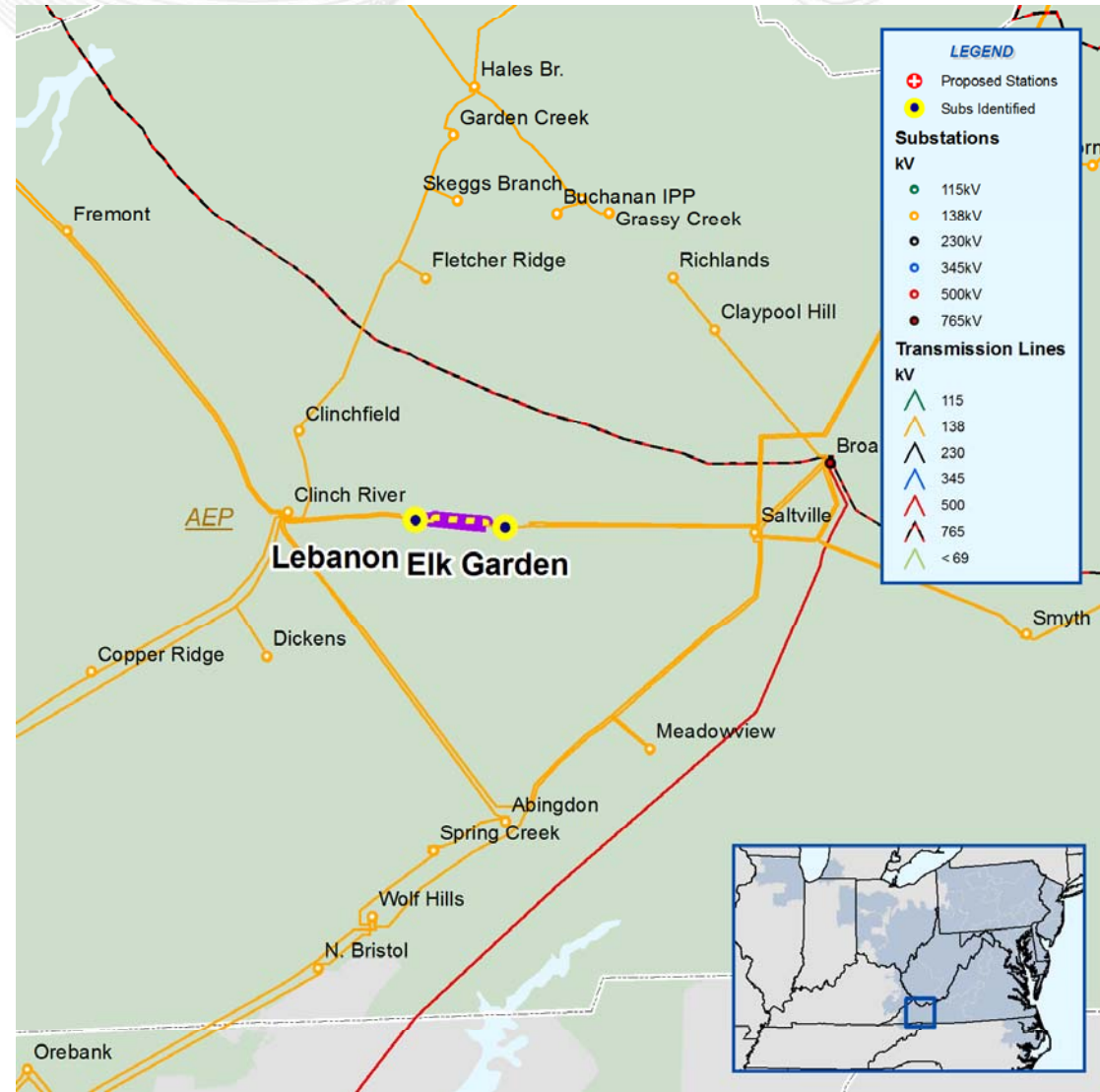
- Potential common mode outage violations
- Greentown 765/138 kV transformer overload for the line with stuck breaker contingency with the loss of the Dumont – Greentown 765 kV line and Greentown three winding transformer



- Potential common mode outage violations
- Grangston – Bellefonte 138 kV line overload for the loss of the Baker 765/345 kV transformer

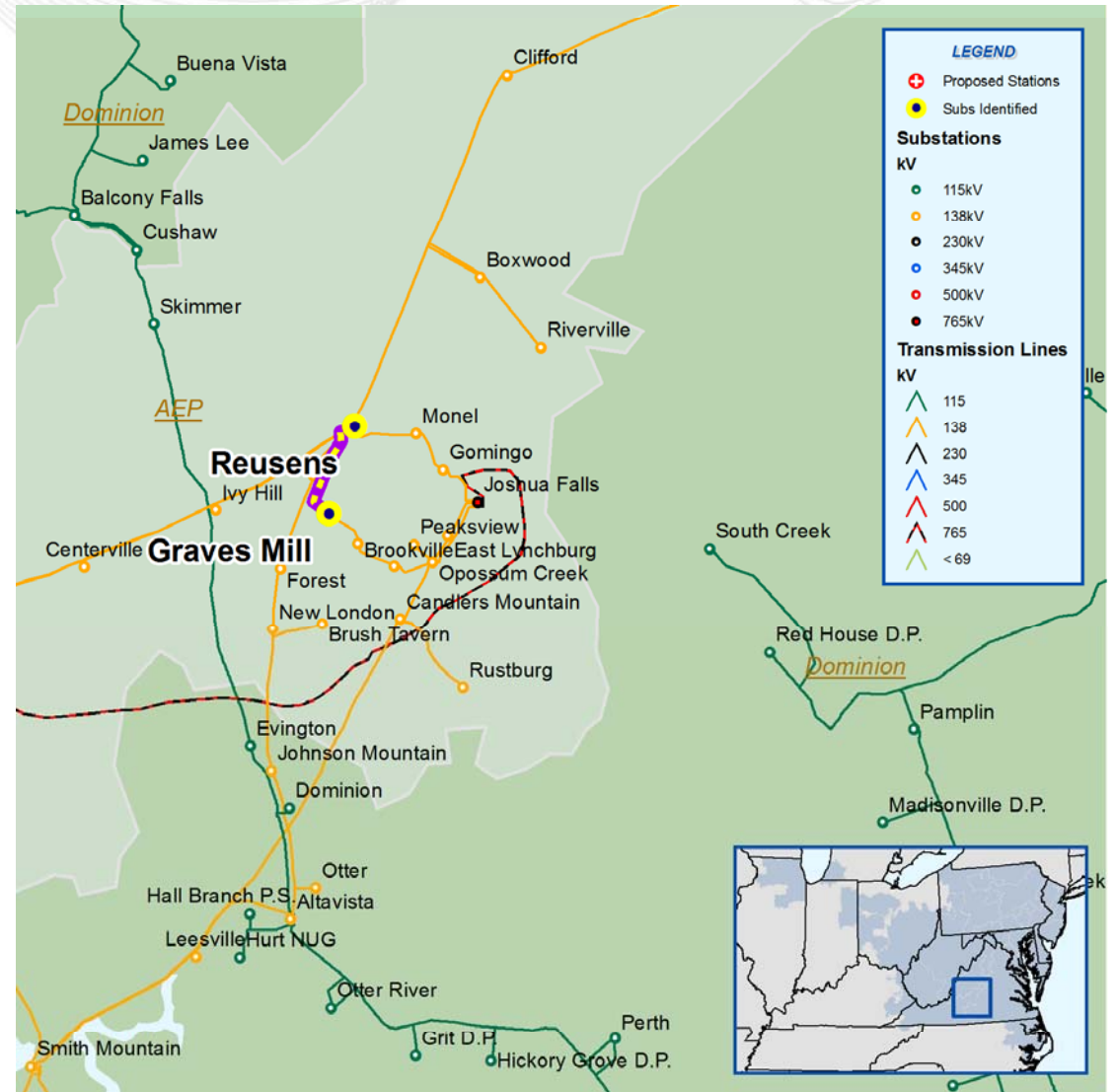


- Potential common mode outage violations
- Lebanon – Elk Garden 138 kV line overload for the tower outage of the Dorton – Fremo 138 kV line and the Flemin – Dorton – Clinch River 138 kV line

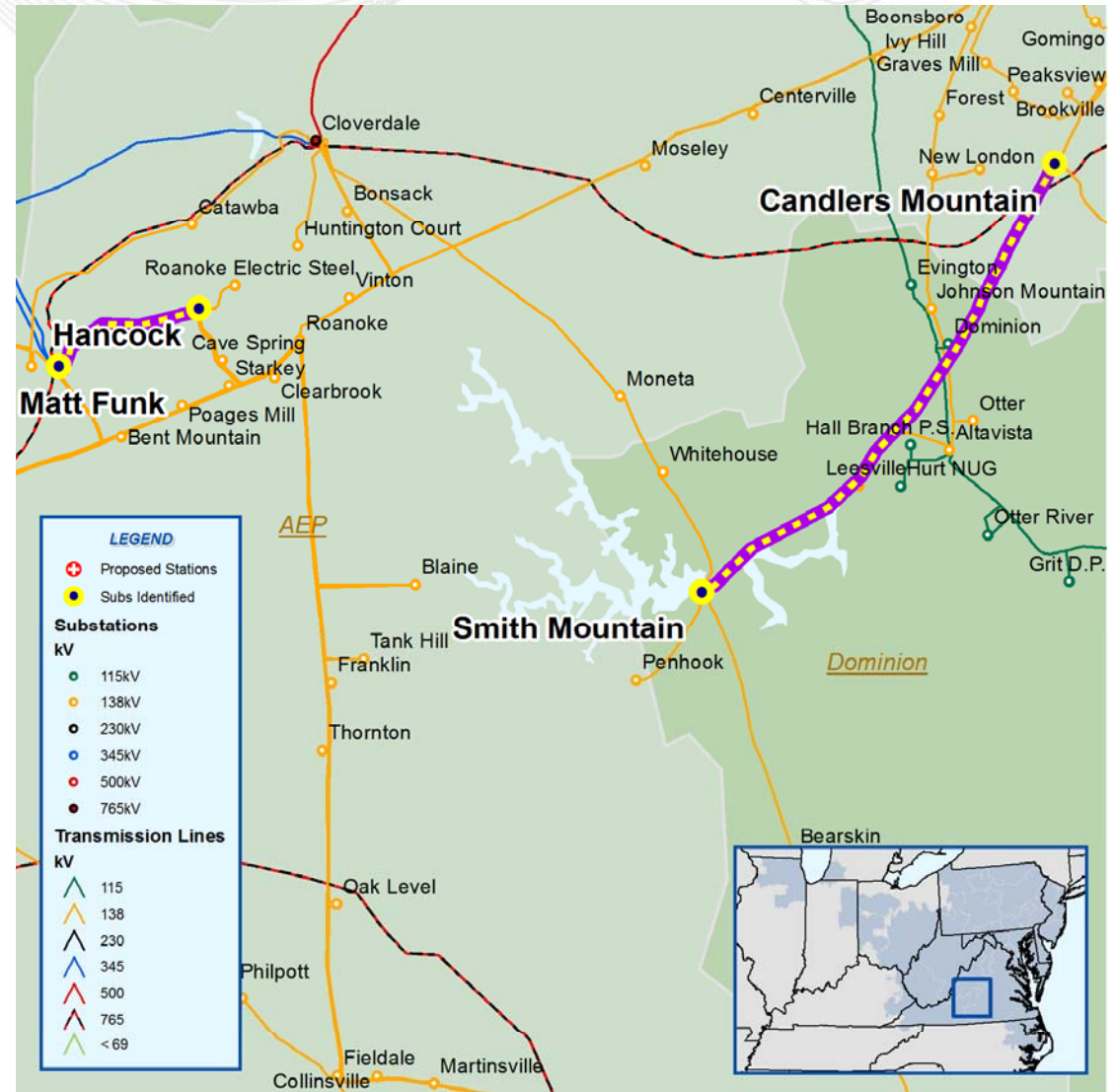




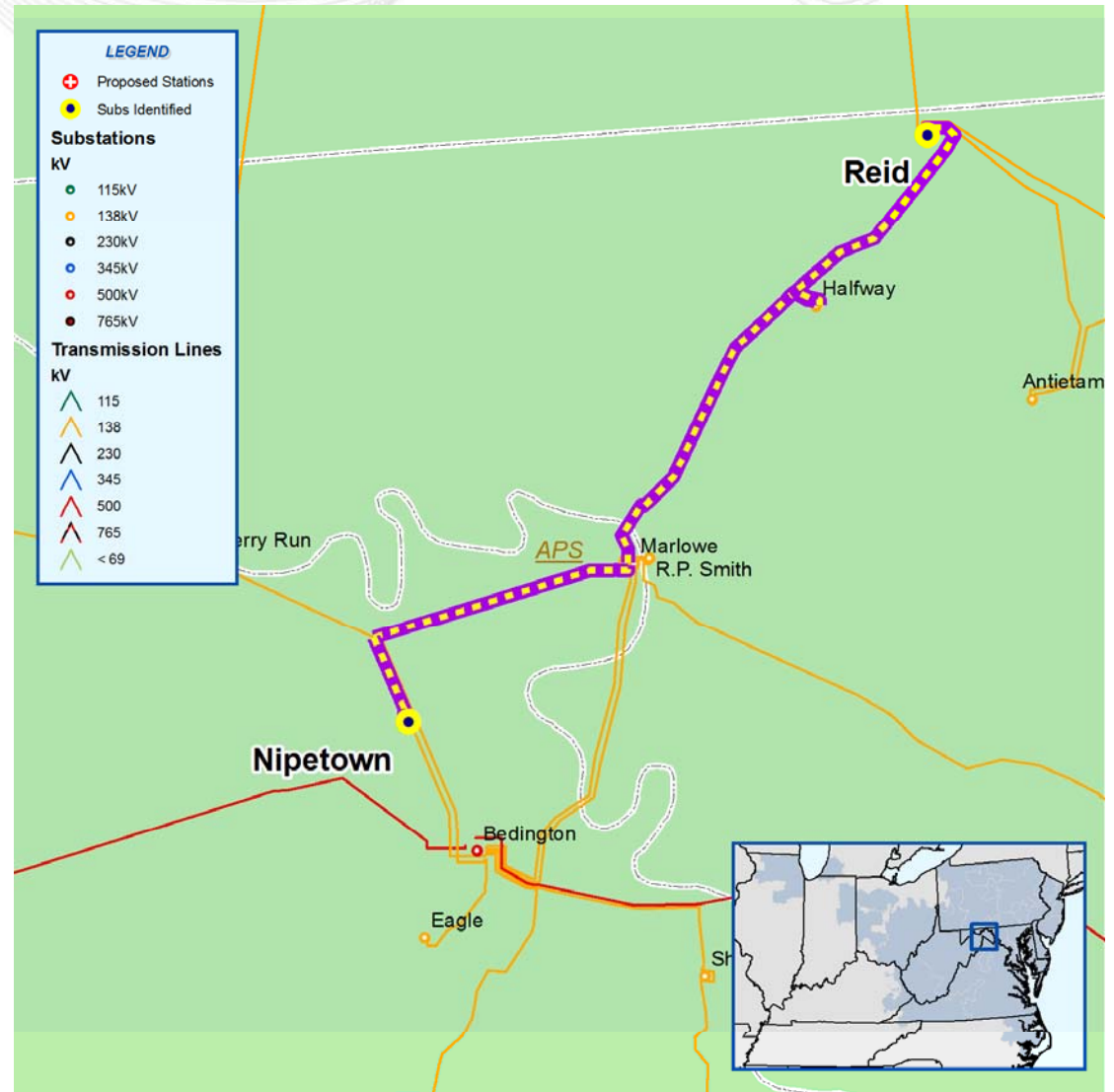
- Potential common mode outage violations
- Reusen – Graves Mill 138 kV line overload for the tower outage of the E. Lynchburg – Joshua 138 kV line and the Joshua – Opossum Creek 138 kV line



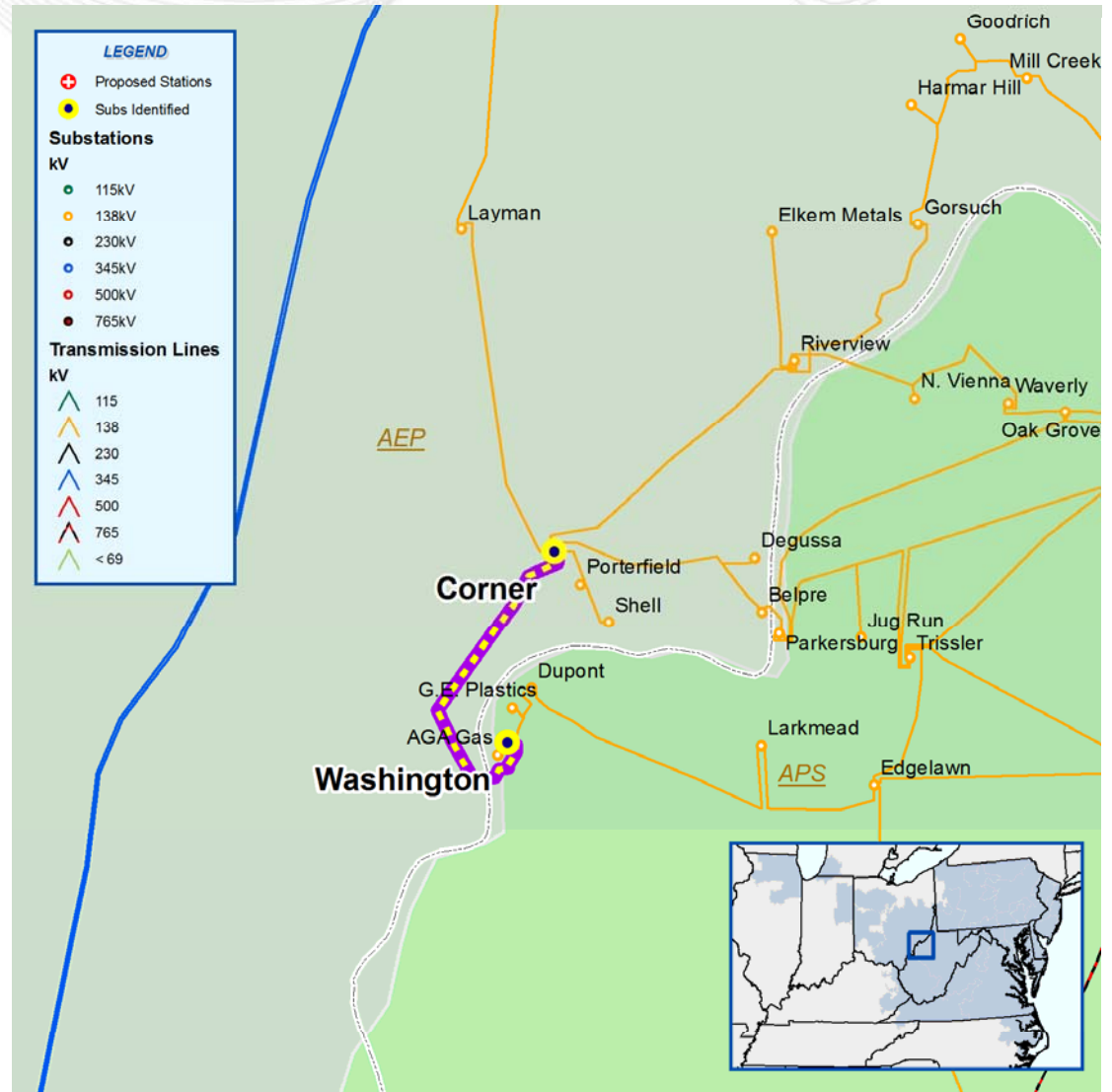
- Potential common mode outage violations
- Smith Mountain – Candler's Mountain 138 kV line overload for several contingencies
- Matt Funk – Hancock 138 kV line overload for the line with stuck break contingency with the loss of Cloverdale – Jacksons Ferry 765 kV line, Cloverdale - Joshua 765 kV line, Cloverdale – Matt Funk 345 kV line



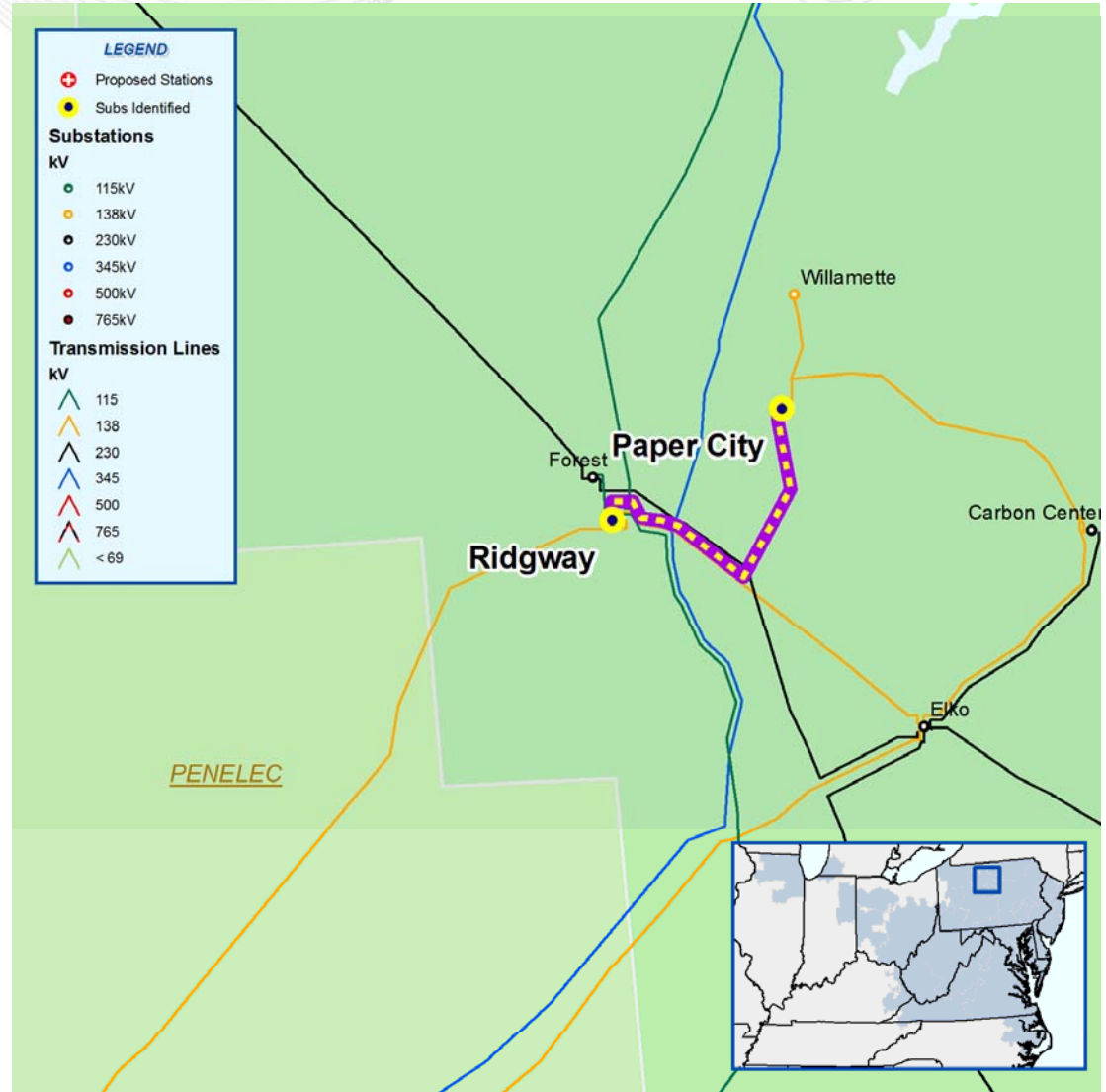
- Potential generator deliverability violations
- For the common mode outage test the Nipetown - Reid 138 kV line is overloaded for the fault of the Marlowe - Harmony Junction 138 kV line with a breaker failure at Marlowe
- Potential Recommended Solution: Reconductor Nipetown - Reid with 1033 ACCR 54/19
- Expected In-Service Date: 06/01/2015



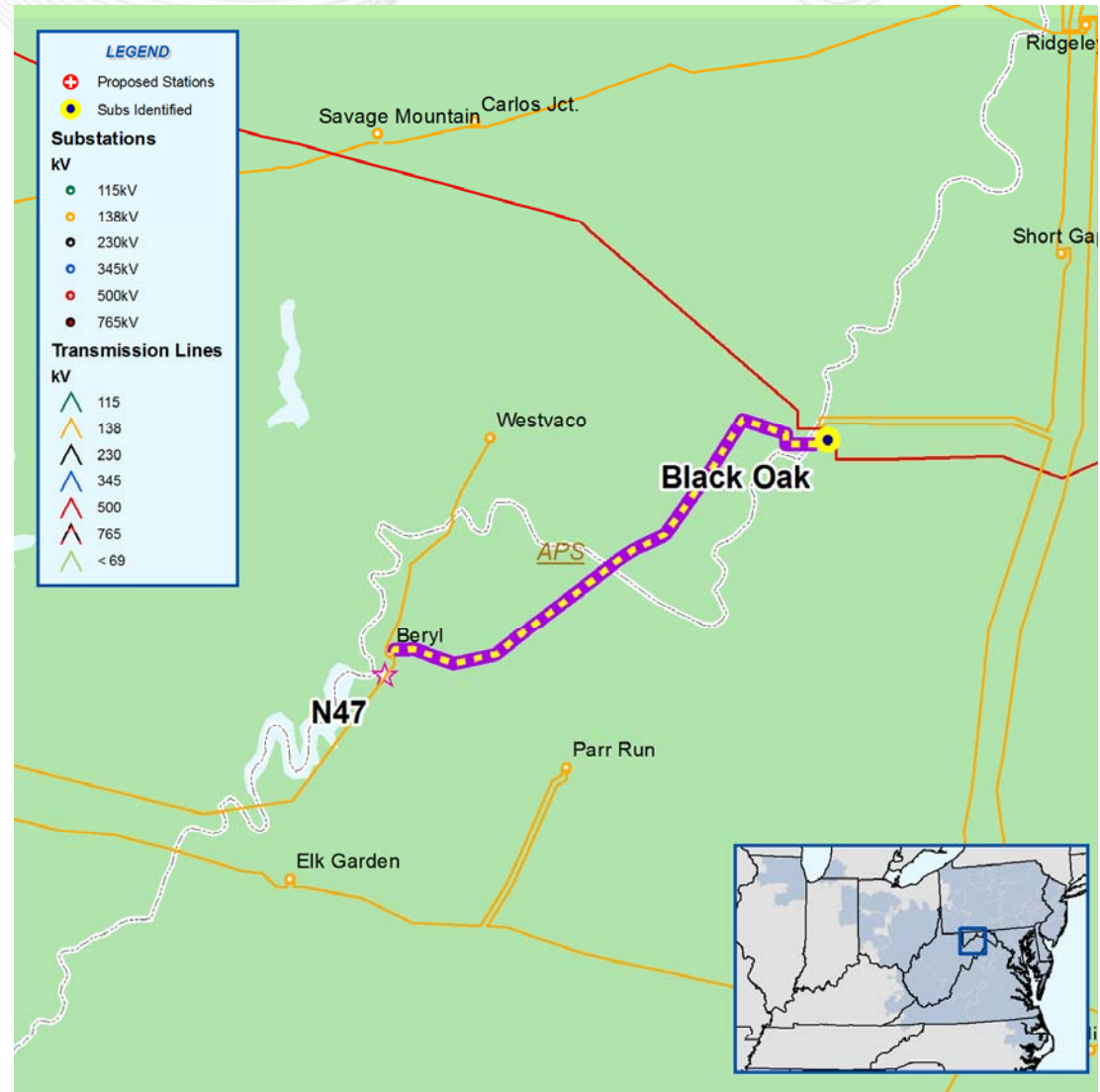
- Potential generator deliverability violations
- Common mode outage violation on Corner - Washington 138 kV line is overloaded for the tower outage of the Belmont – Trissler 138 kV line #1 and the Belmont – Edgelawn 138 kV line
- Potential Recommended Solution: Upgrade Terminal Equipment at Washington 138kV
- Expected In-Service Date: 06/01/2015



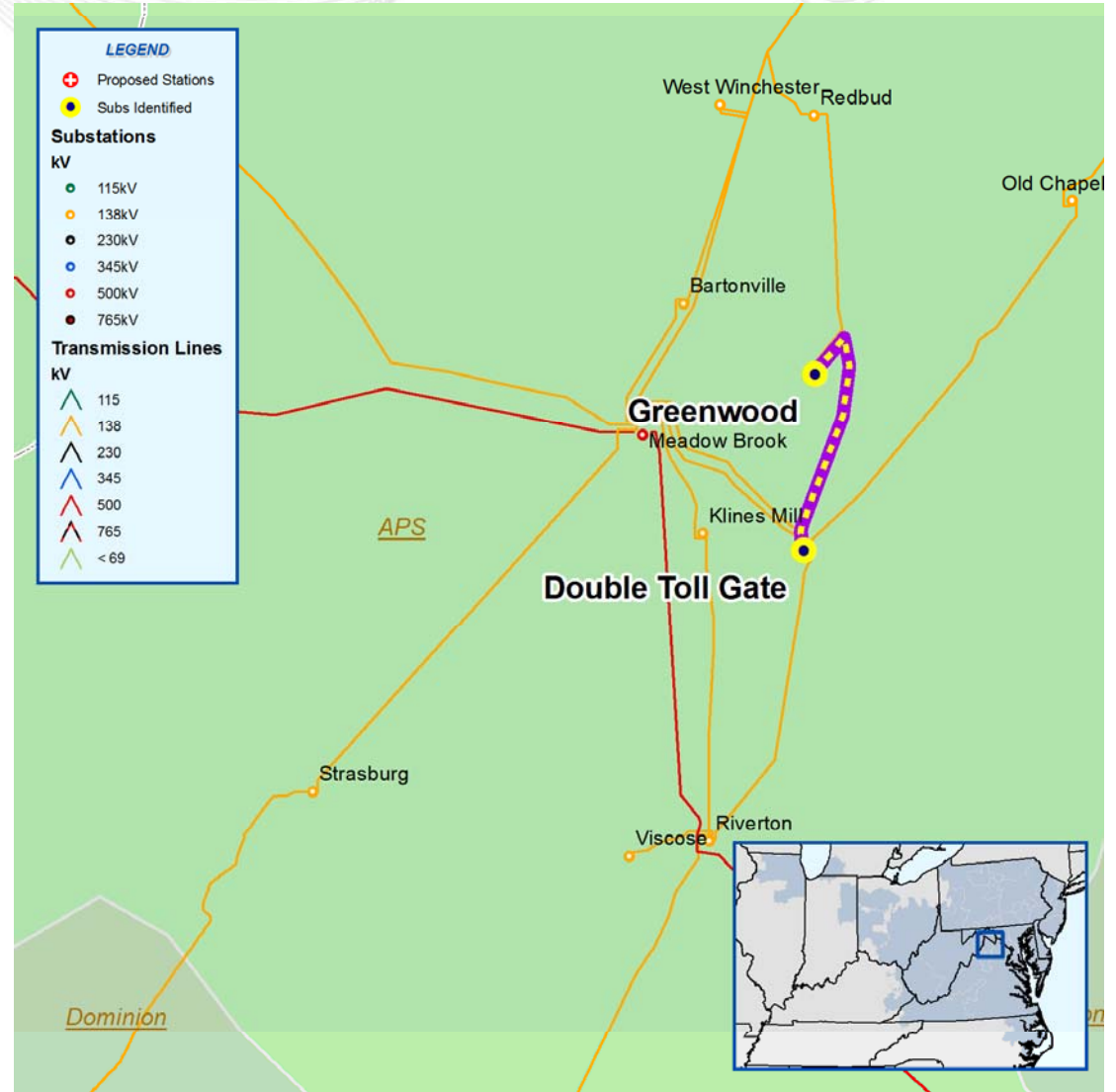
- Potential generator deliverability violations
- For the common mode outage test the Ridgeway – Paper City 138 kV line is overloaded for the tower outage of the Elko 230 kV #4 Breaker Failure - Tie Breaker
- Potential Recommended Solution: Replace Structures between Ridgeway and Paper City
- Estimated In-Service Date: 06/01/2015



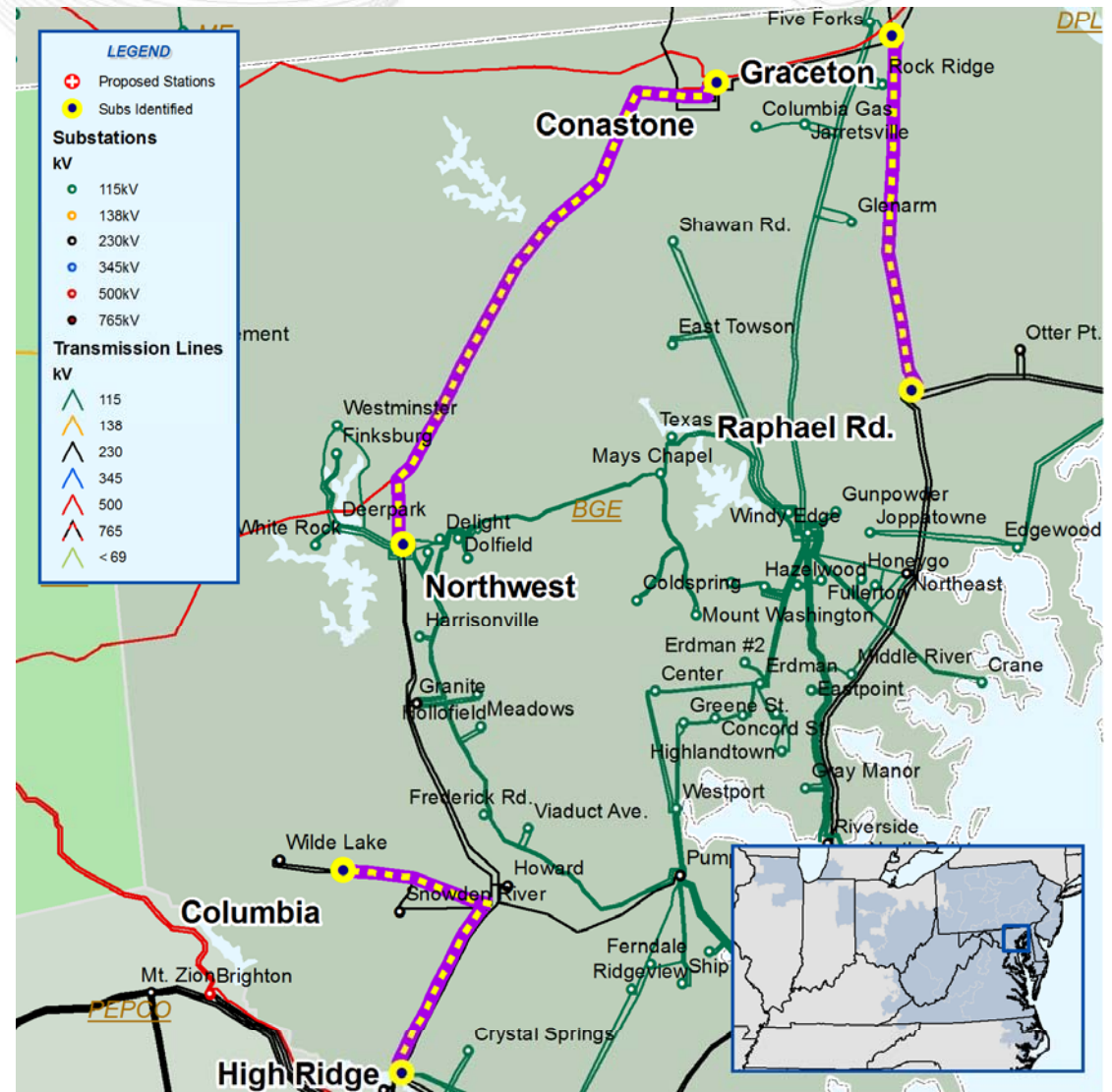
- Potential generator deliverability violations
- Common mode outage violation on the N47 Tap – Black Oak 138 kV line is overloaded for the Black Oak – Hatfield 500 kV line fault with stuck breaker Black Oak #4 or Black Oak500 #5
- Potential Recommended Solution: Reconductor the Albright - Black Oak 138 kV line with 795 ACSS
- Expected In-Service Date : 06/01/2015



- Potential generator deliverability violations
- For the generator deliverability test the Double Tollgate - Greenwood 138 kV line is overloaded for the loss of the Meadow Brook – West Winchester 138 kV line
- Potential Recommended Solution: Reconductor Double Toll Gate - Greenwood 138 kV with 954 ACSR conductor
- Expected In-Service Date: 06/01/2013

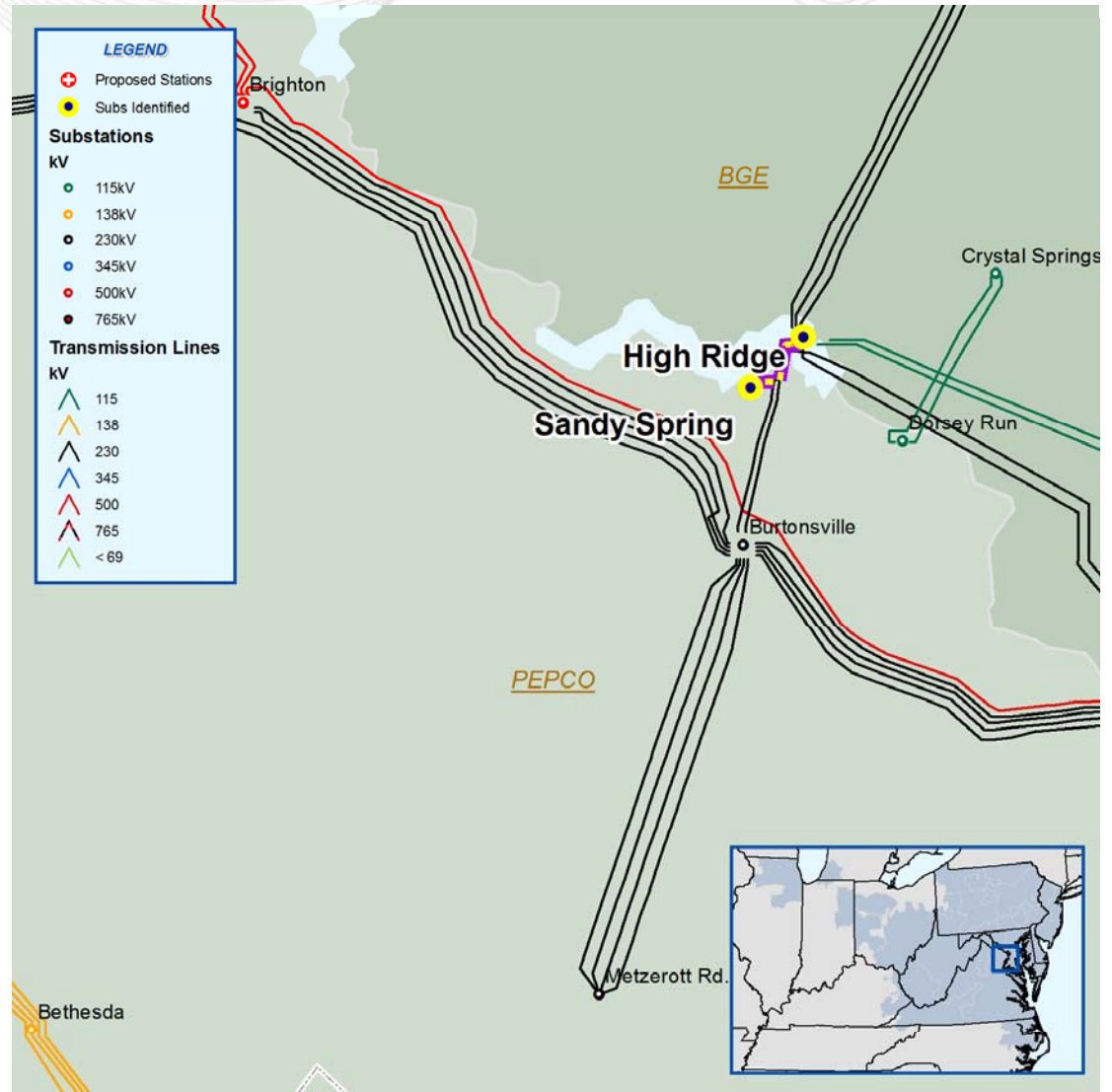


- Potential Common Mode Outage violations
- The Graceton – Bagley – Raphael 230 kV circuit is overloaded for the Conastone to North West 230 kV tower line outage
- The Conastone – North West 230 kV circuit (2322) is overloaded for the Brighton – Conastone, Brighton – Doubs 500 kV tower line outage
- The High Ridge – Columbia 230 kV circuit (2312) is overloaded for the Conastone to North West 230 kV tower line outage

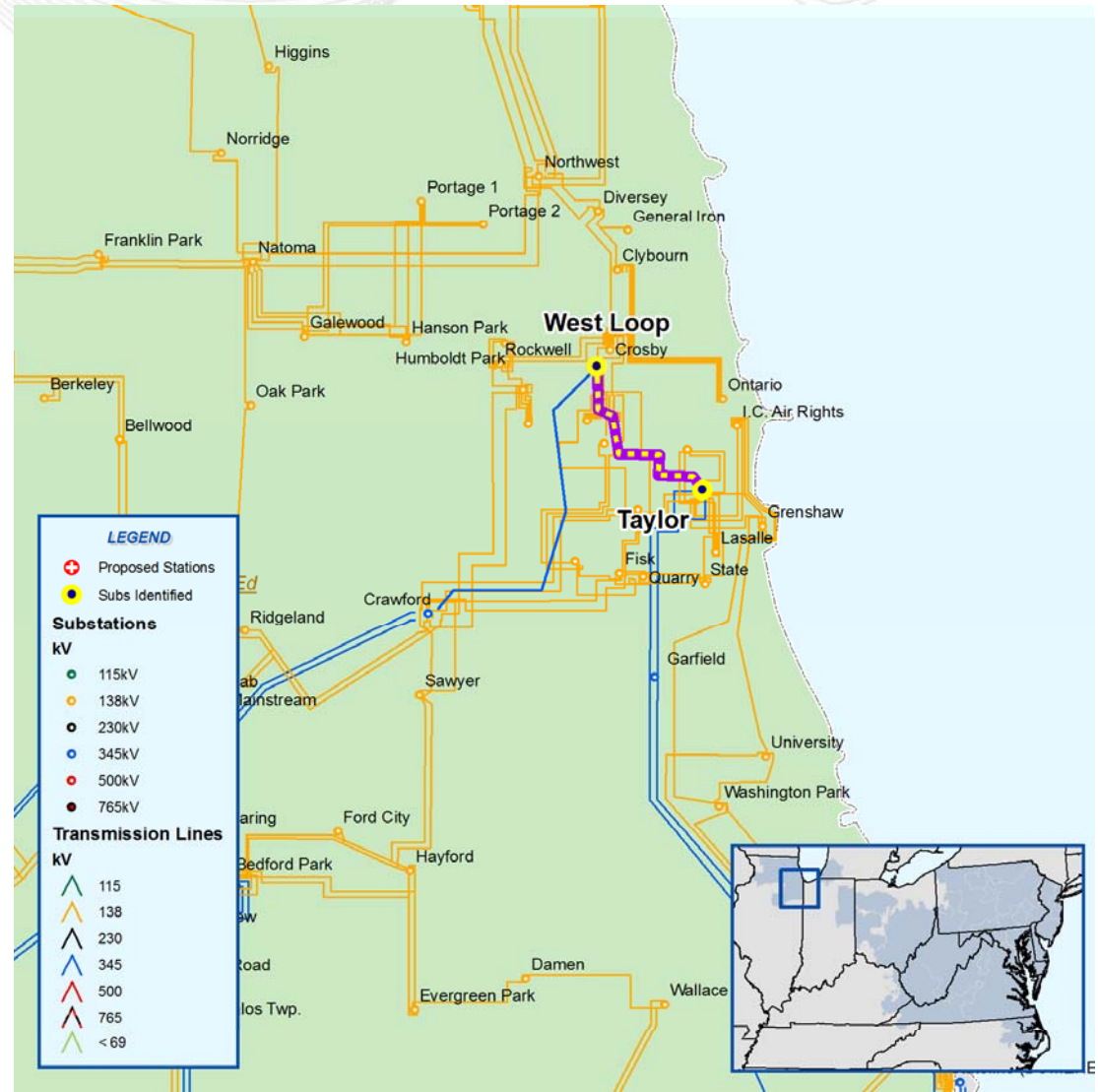




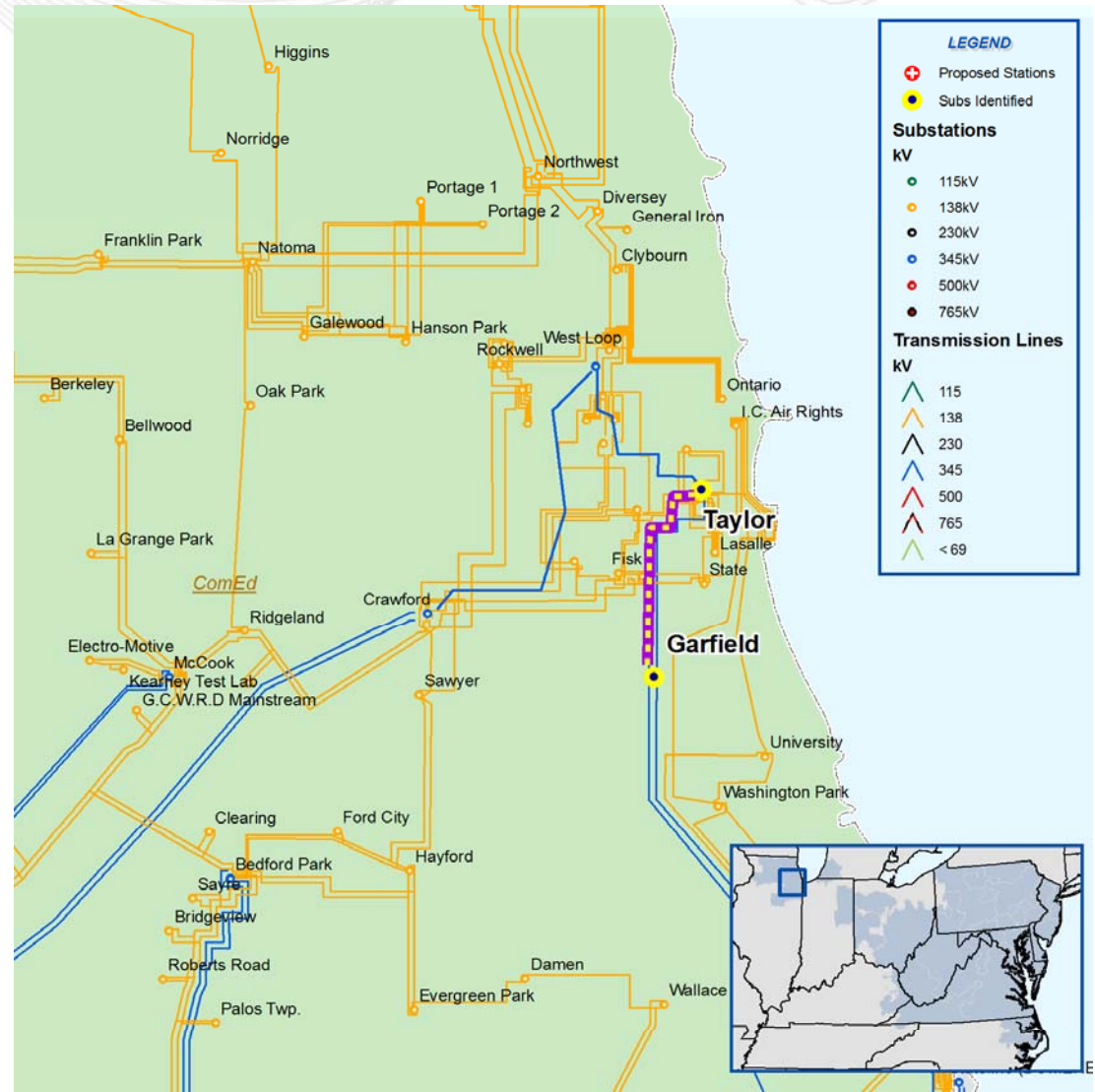
- Potential Generation Deliverability violation
- The Sandy Spring – High Ridge 230 kV circuit (2334) is overloaded for loss of the Sandy Spring to Burtonsville 230 kV circuit (2314)
- The Sandy Spring – High Ridge 230 kV circuit (2314) is overloaded for loss of the Sandy Spring to Burtonsville 230 kV circuit (2334)



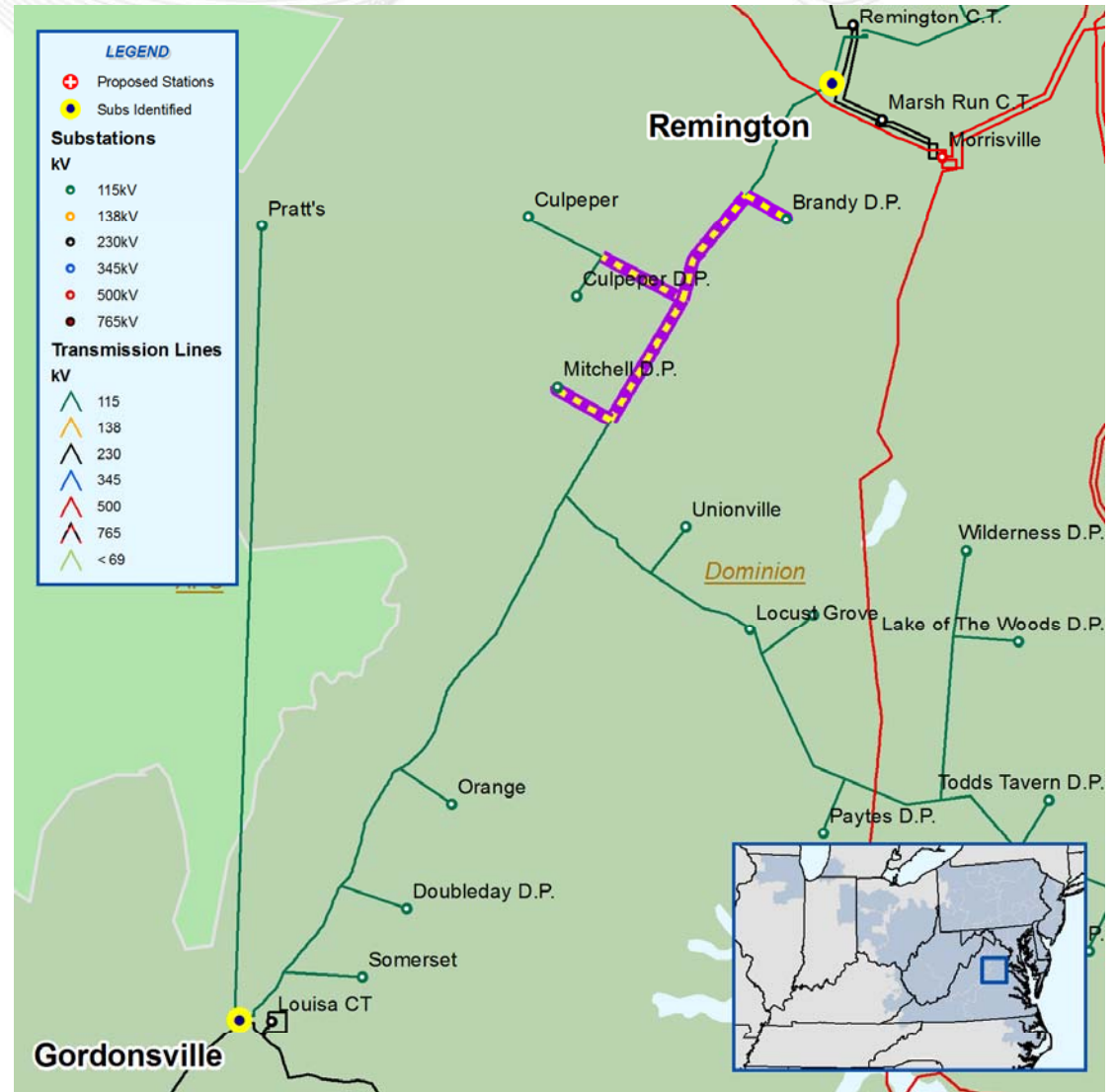
- Potential common mode outage violations
- Taylor – West Loop 345 kV Blue line is overloaded for the common tower contingency with loss of the line #1311 and line #1312
- Lisle Blue 345/138 kV transformer is overloaded for several contingencies



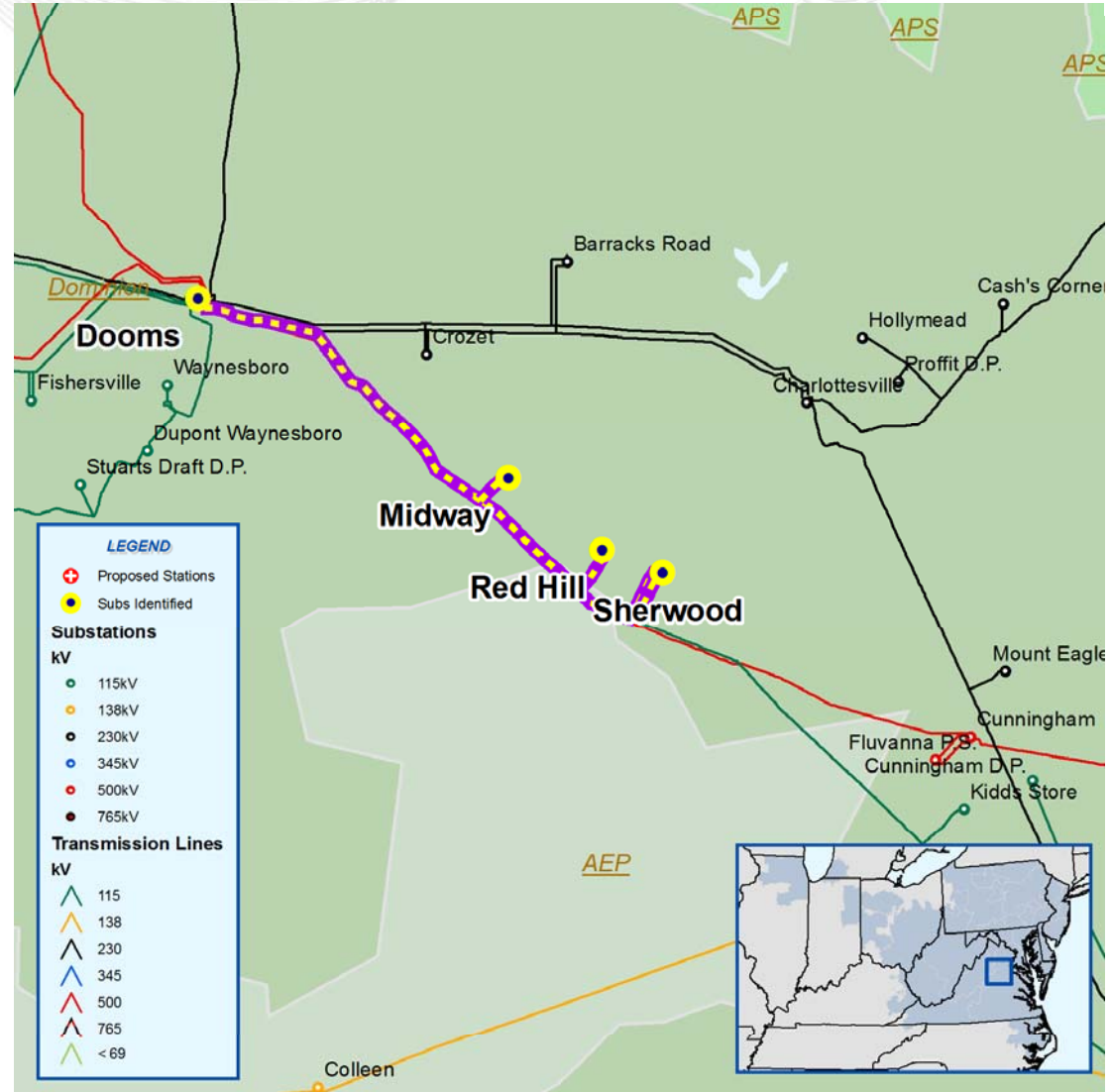
- Potential generator deliverability violation
- Garfield – Taylor 345 kV red is overloaded for the normal system condition
- East Frankfort – Goodings Grove 345 kV red is overloaded for the normal system condition



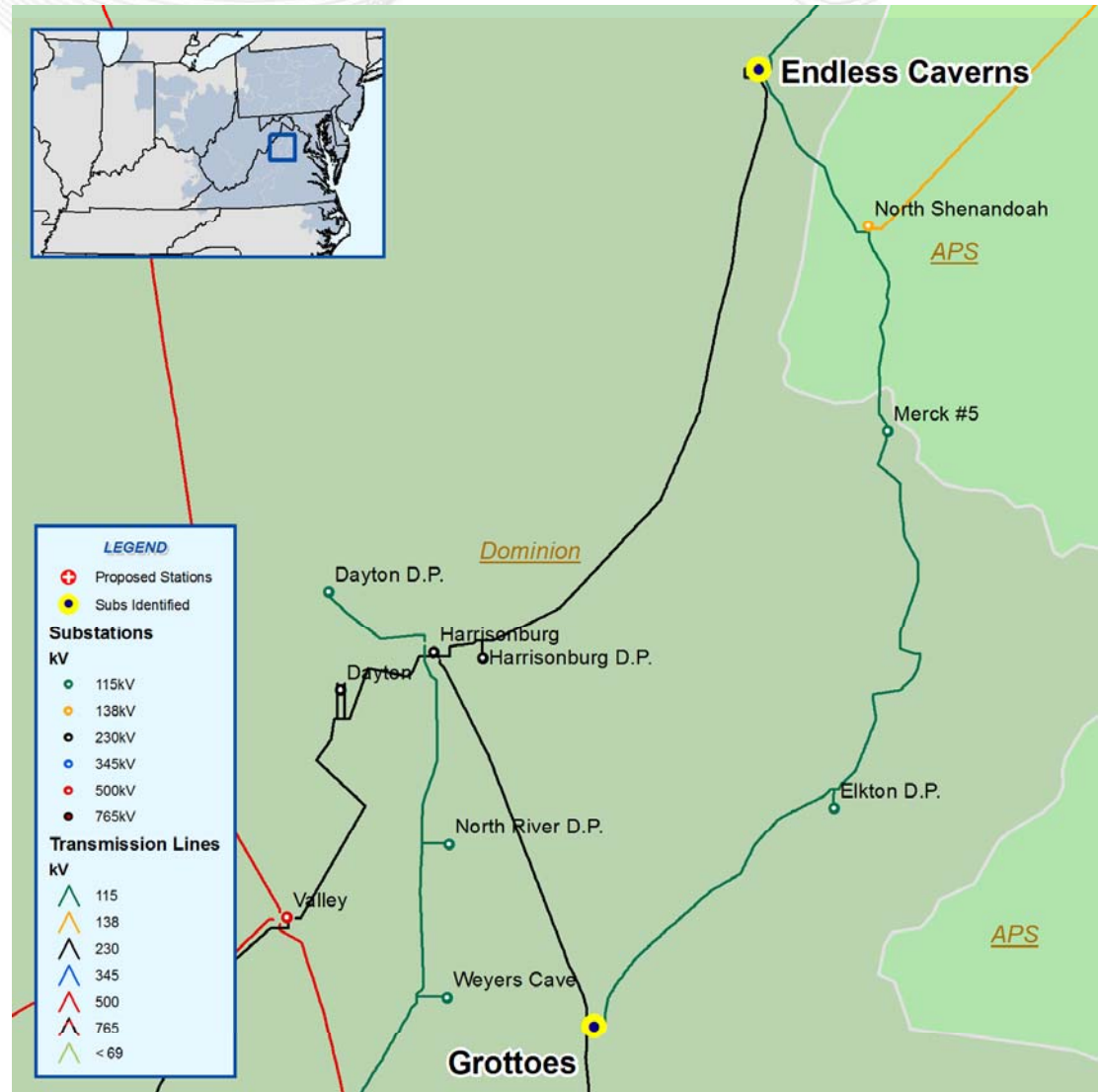
- Potential voltage violation for the common mode outage test
- The Gordonsville 230/115 kV Transformer #1 overloads for the outage of transformer #2
- A line fault with stuck breaker at Remington 230 kV causes low voltage magnitude violations in the Brandy - Culpeper - Mitchell 115 kV area



- Potential voltage violation for the common mode outage test
- A bus fault at Dooks 115 kV results in low voltage magnitude violations in the Midway - Red Hill - Sherwood 115 kV area



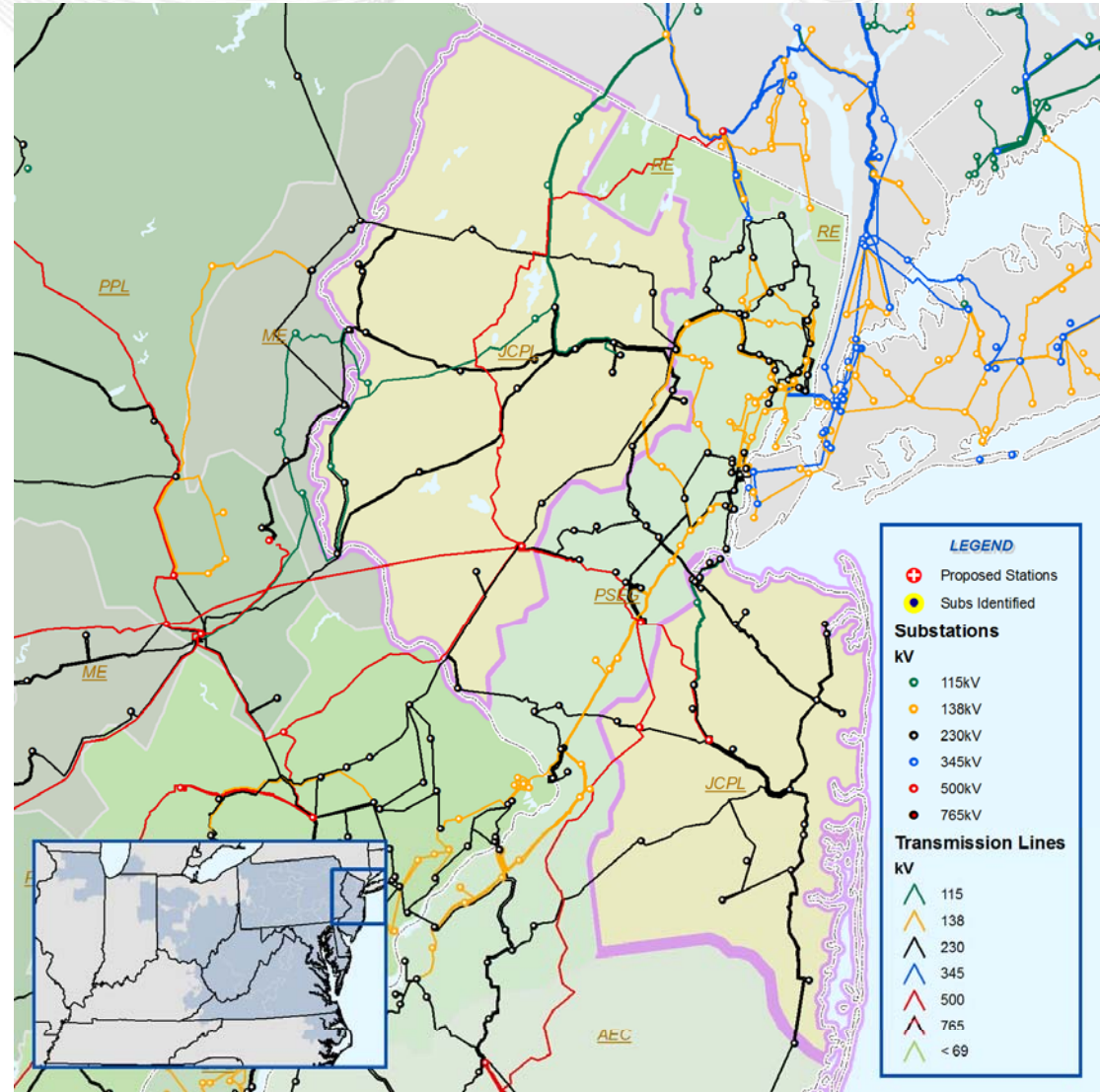
- Potential generator deliverability violation
- The Endless Caverns 230/115 kV transformer overloads for the outage of the Grottoes 230/115 kV transformer



- Potential Common Mode Outage violation
- The Raritan River – Deep Run 115 kV ‘B’ and ‘C’ circuits are overloaded for a line fault stuck breaker contingency that outages the Smithburg – Atlantic and Smithburg – Englishtown 230 kV circuits

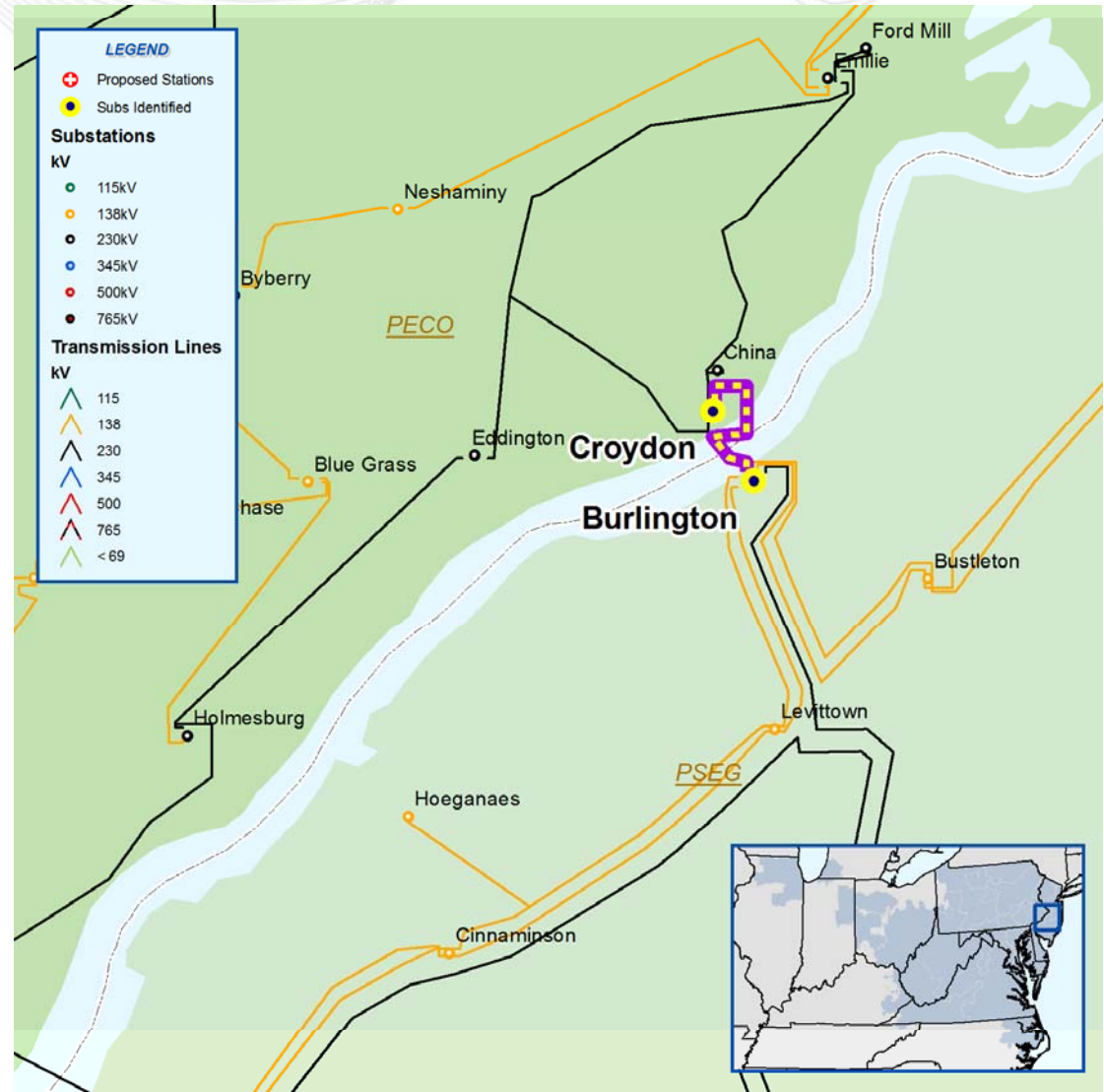


- Potential Load Deliverability violation
- JCPL zonal load deliverability analysis shows voltage collapse violations for several contingencies in JCPL area

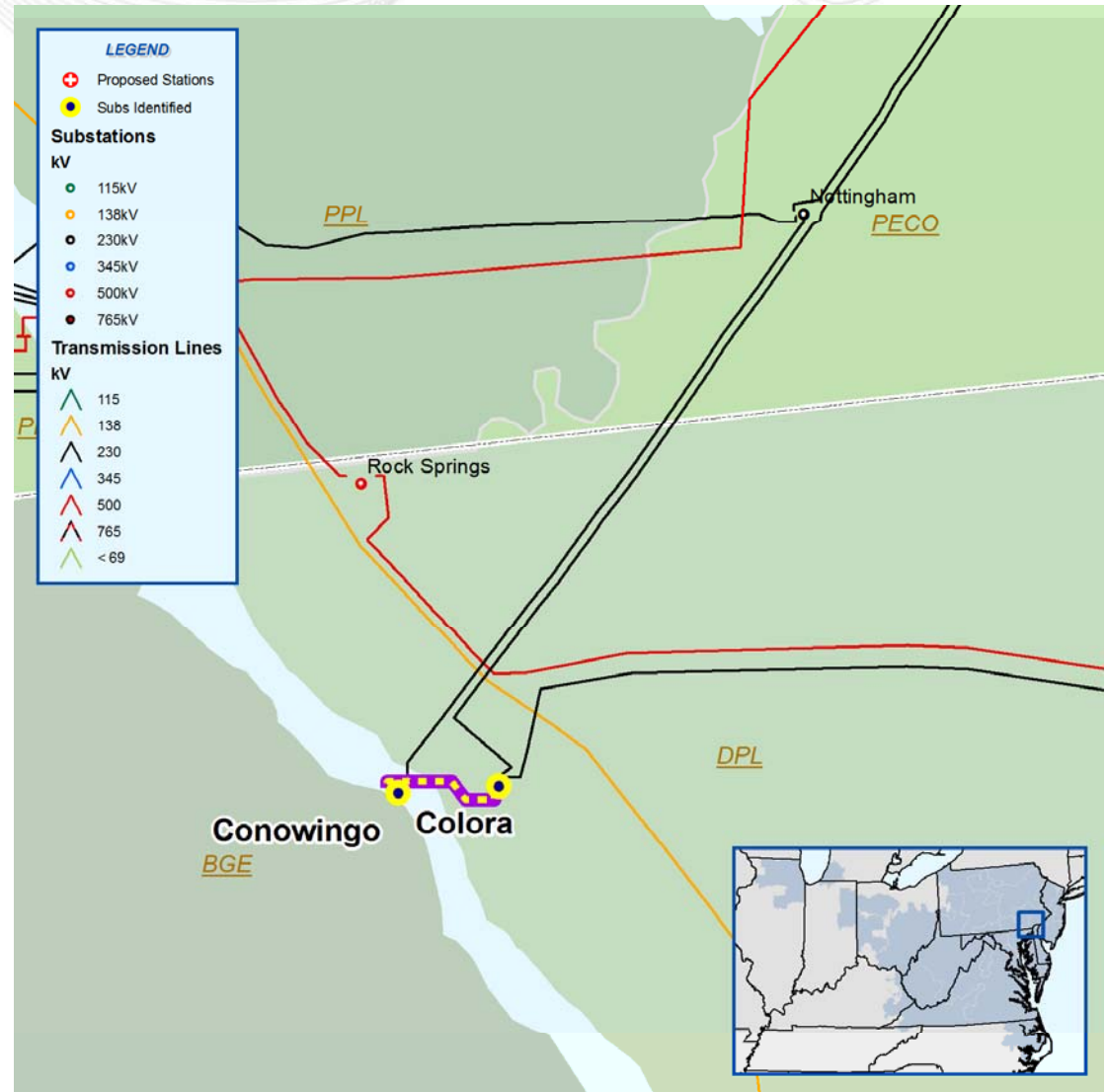




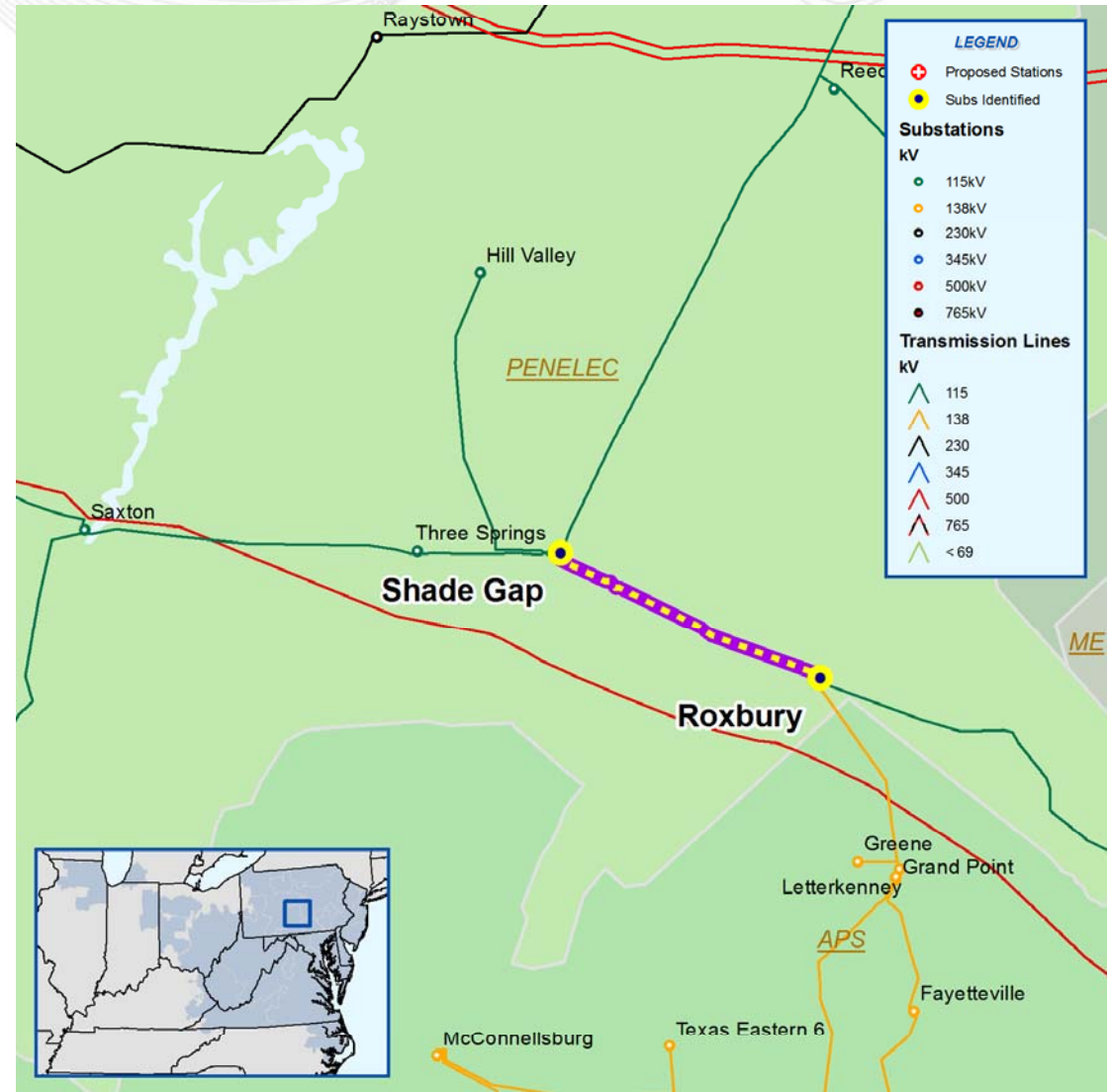
- Potential Generation Deliverability violation
- The Croydon – Burlington 230 kV circuit is overloaded for several contingencies



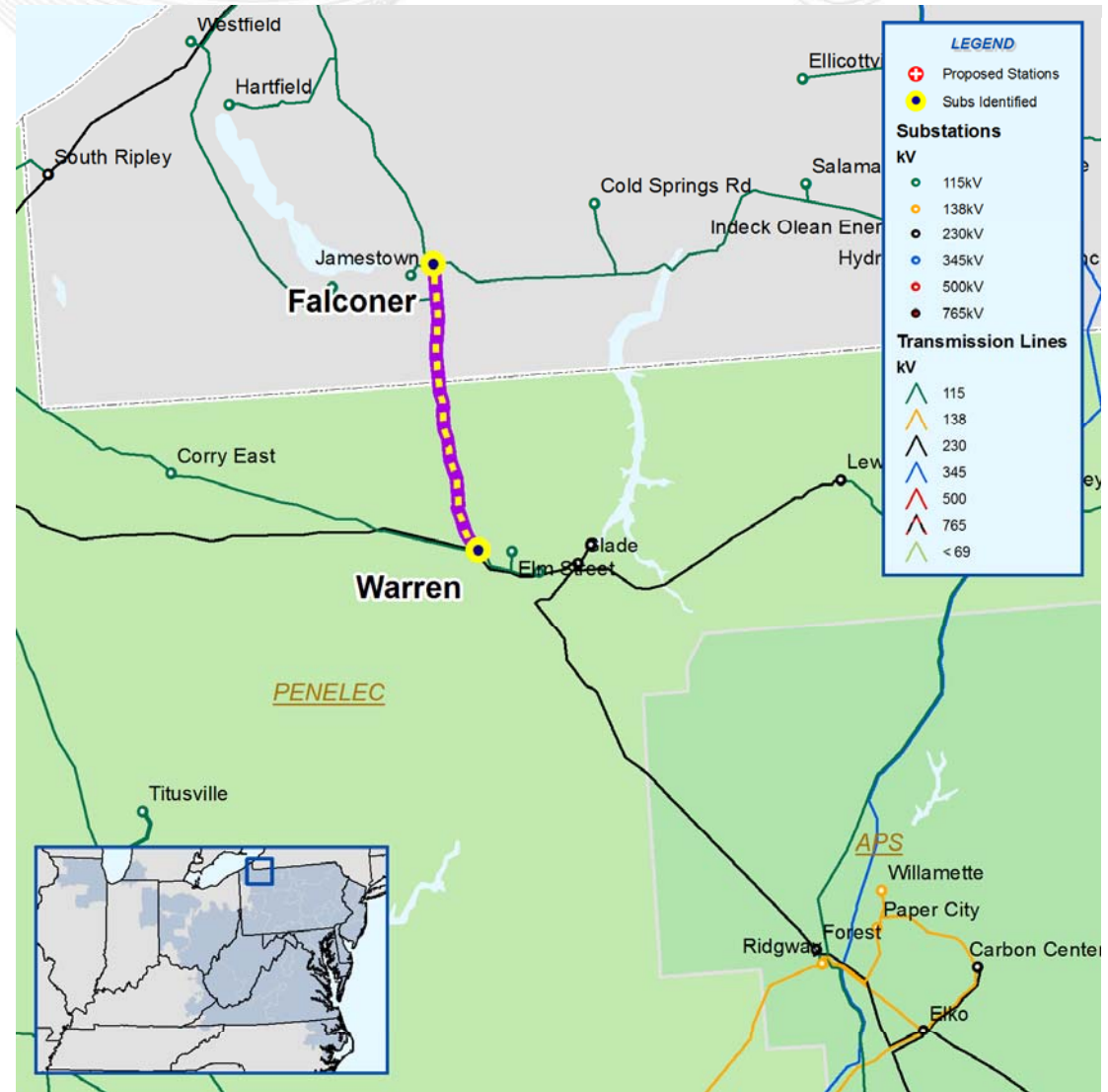
- Potential Generation Deliverability violation
- The Conowingo – Colora Tap 230 kV circuit is overloaded for the loss of the Conowingo – Nottingham 230 kV circuit



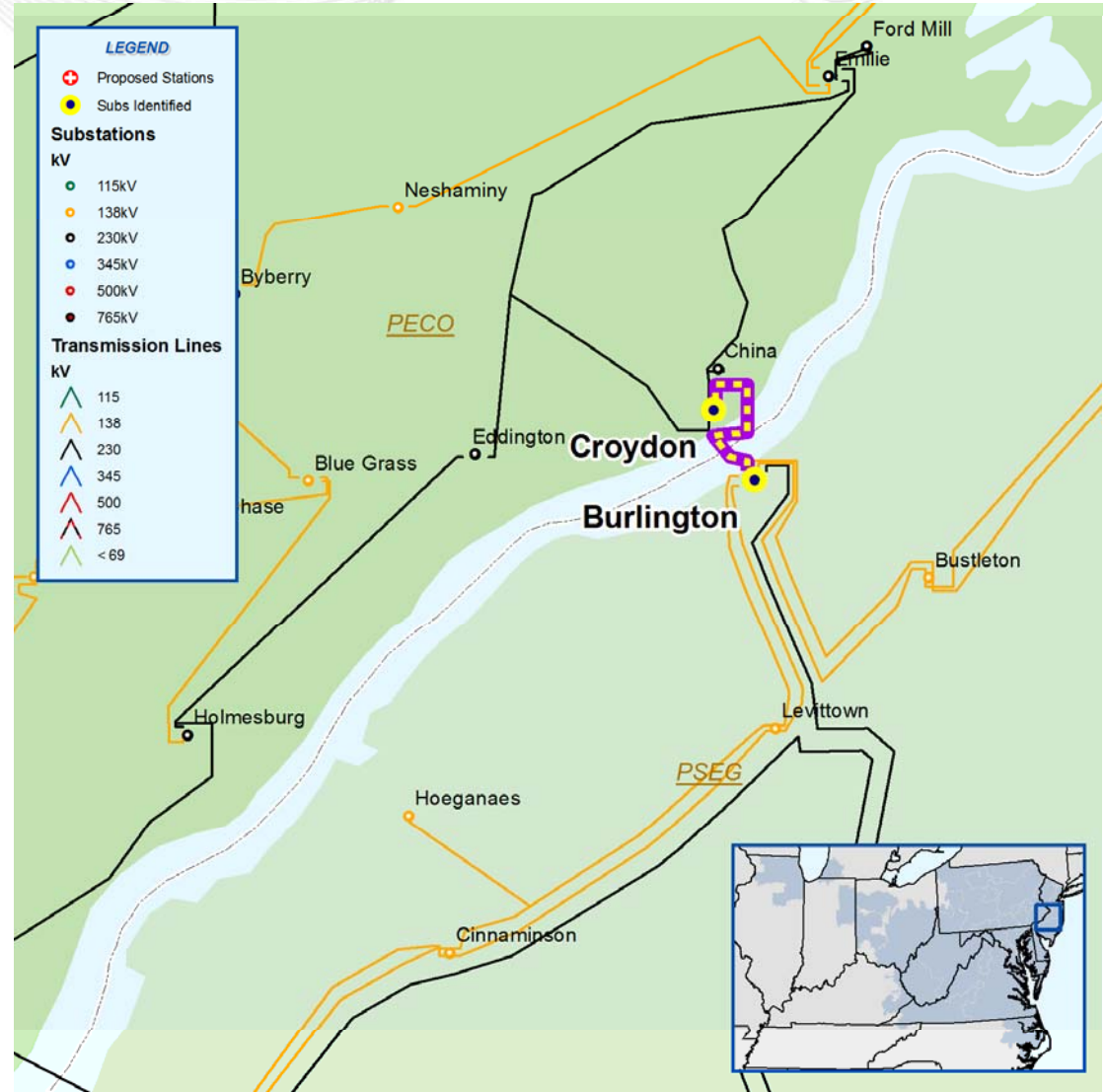
- Potential Generation Deliverability violation
- The Shade Gap – Roxbury 115 kV circuit is overloaded for several contingencies



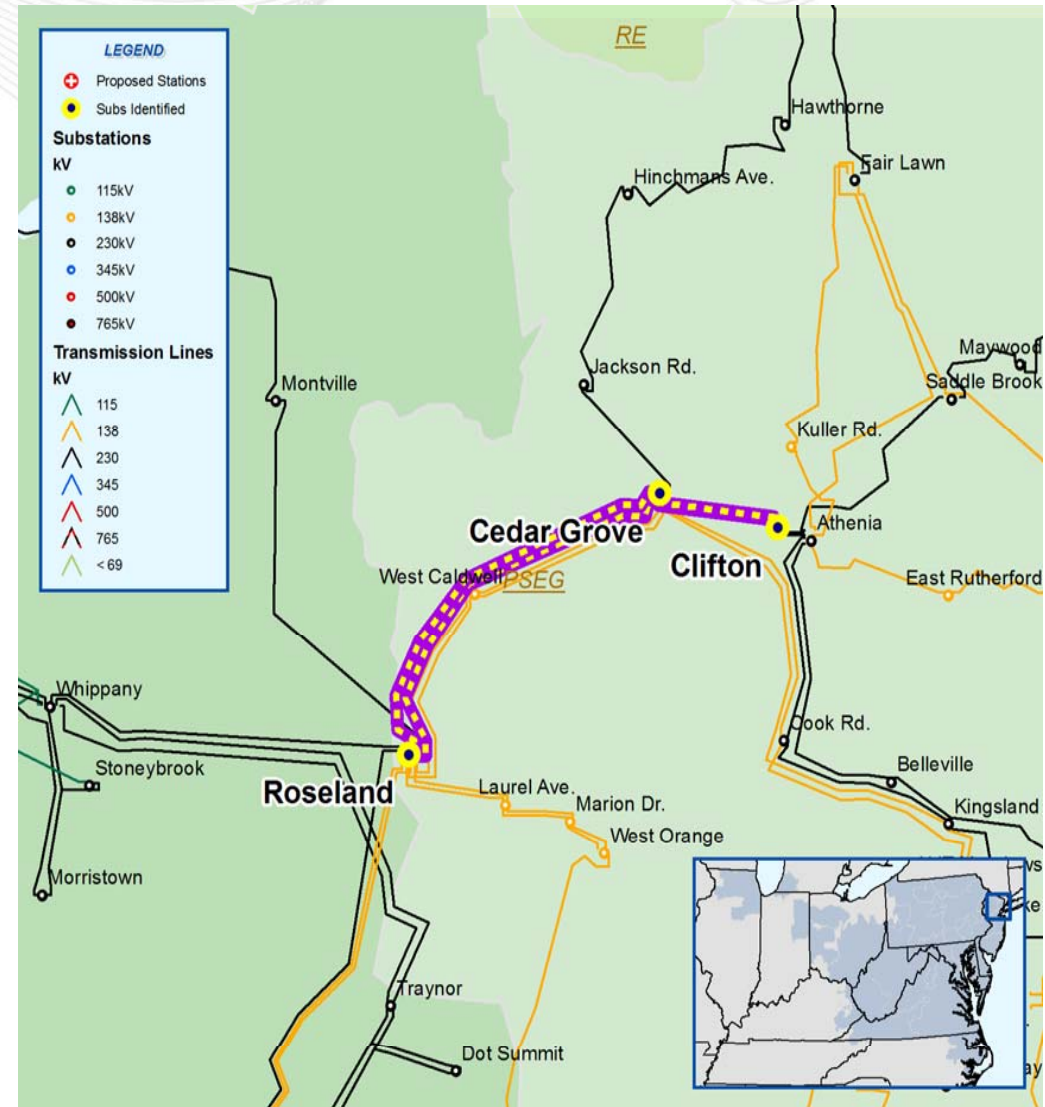
- Potential Common Mode Outage violation
- The Warren – Falconer 115 kV circuit is overloaded for the Glade – Forest, Glade – Lewis Run 230 kV tower line outage



- Potential Generation Deliverability violation
- The Croydon – Burlington 230 kV circuit is overloaded for several contingencies
- The Gloucester – Cuthbert 230 kV circuit is overloaded for several contingencies
- Cuthbert – Camden 230 kV circuit is overloaded for several contingencies
- Eagle Point – Gloucester 230 kV is overloaded for several contingencies



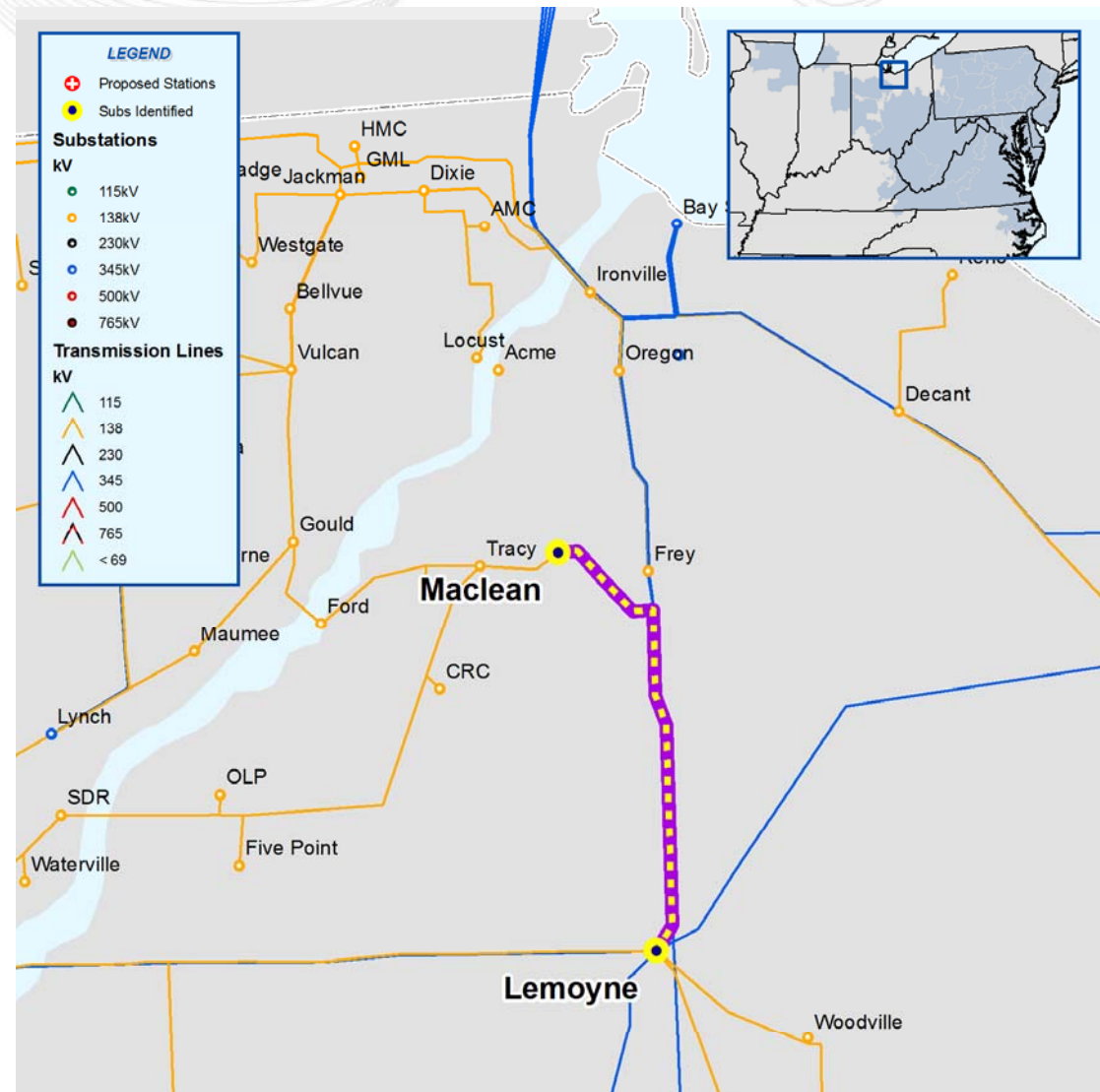
- Potential Load Deliverability violation
- PSEG and PS North Zonal load Deliverability
- The Roseland – Cedar Grove – Clifton 230 kV ‘B’ and circuit is overload for the loss of the Roseland – Cedar Grove – Clifton 230 kV ‘F’ circuit
- The Roseland – Cedar Grove – Clifton 230 kV and ‘F’ circuit is overload for the loss of the Roseland – Cedar Grove – Clifton 230 kV ‘B’ circuit
- Voltage collapse violations for few 500 kV contingencies for PSEG load deliverability





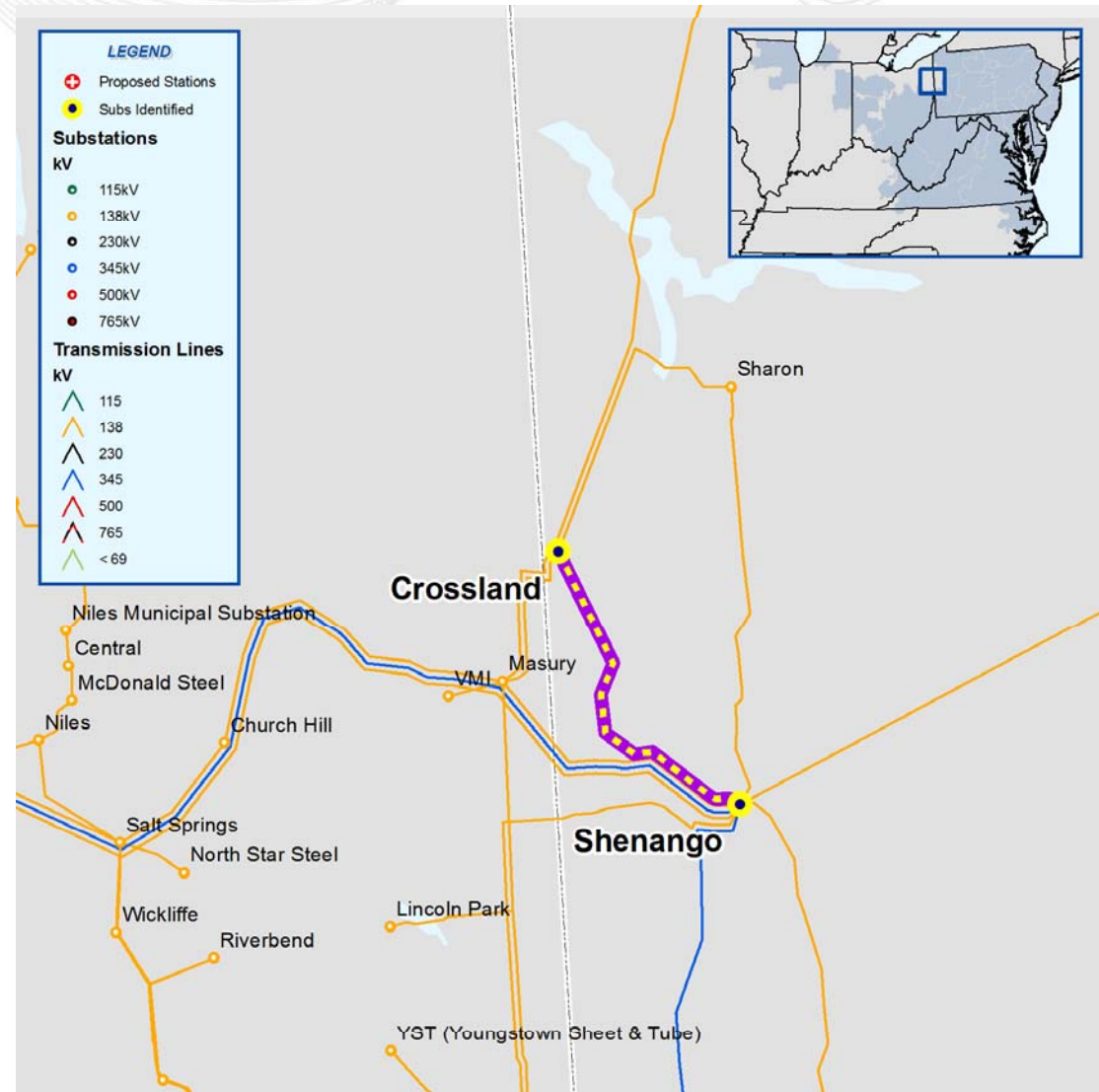
# Baseline Reliability Update

- For the common mode outage test the Lemoyne – Maclean 138 kV circuit is overloaded for breaker failure operation of Bayshore 138 kV BK-JL Breaker
- Recommended Solution: Reconductor Lemoyne – Maclean with 954 ACSS conductor (B1190)
- Estimated Cost: \$4.3M
- Expected In-Service Date: 06/01/2013



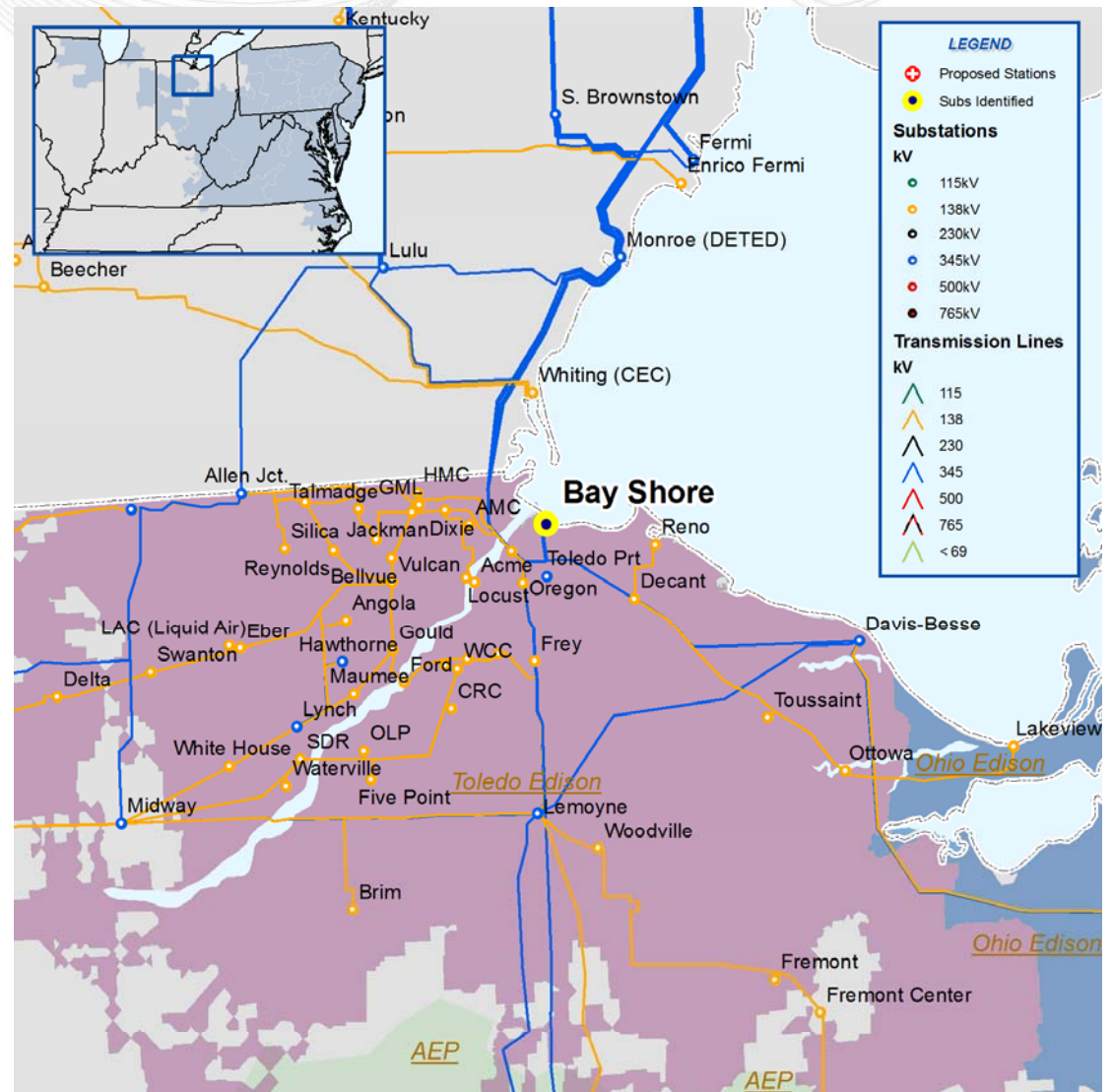


- For the common mode outage test the Shenango – Crossland 138 kV circuit #2 is overloaded for breaker failure operation of Shenango 138 kV BK-18 Breaker
- Recommended Solution: Replace the meter at Crossland with a higher rated meter (B1191)
- Estimated Cost: \$0.015M
- Expected In-Service Date: 06/01/2013

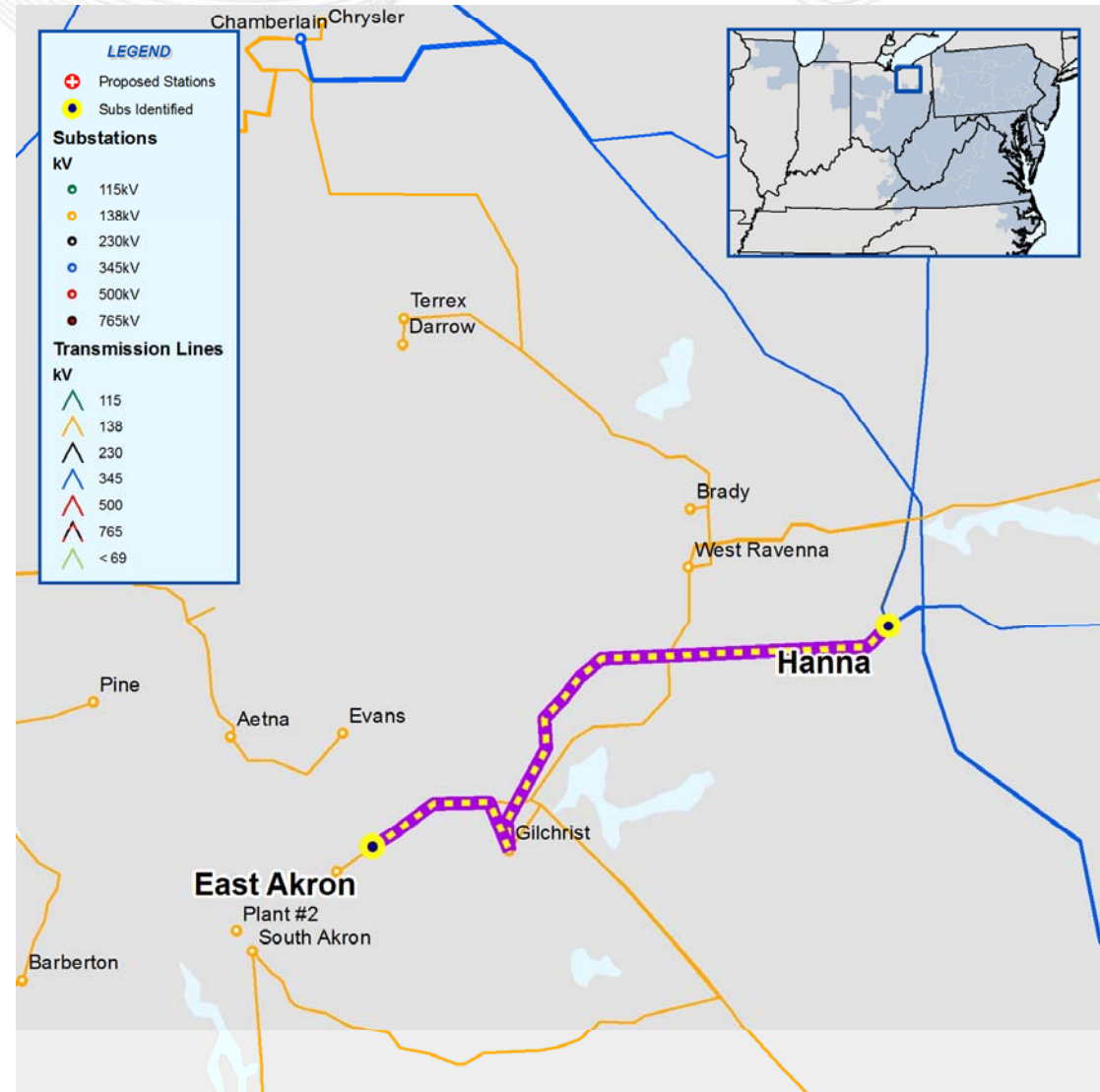


# ATSI Transmission Zone

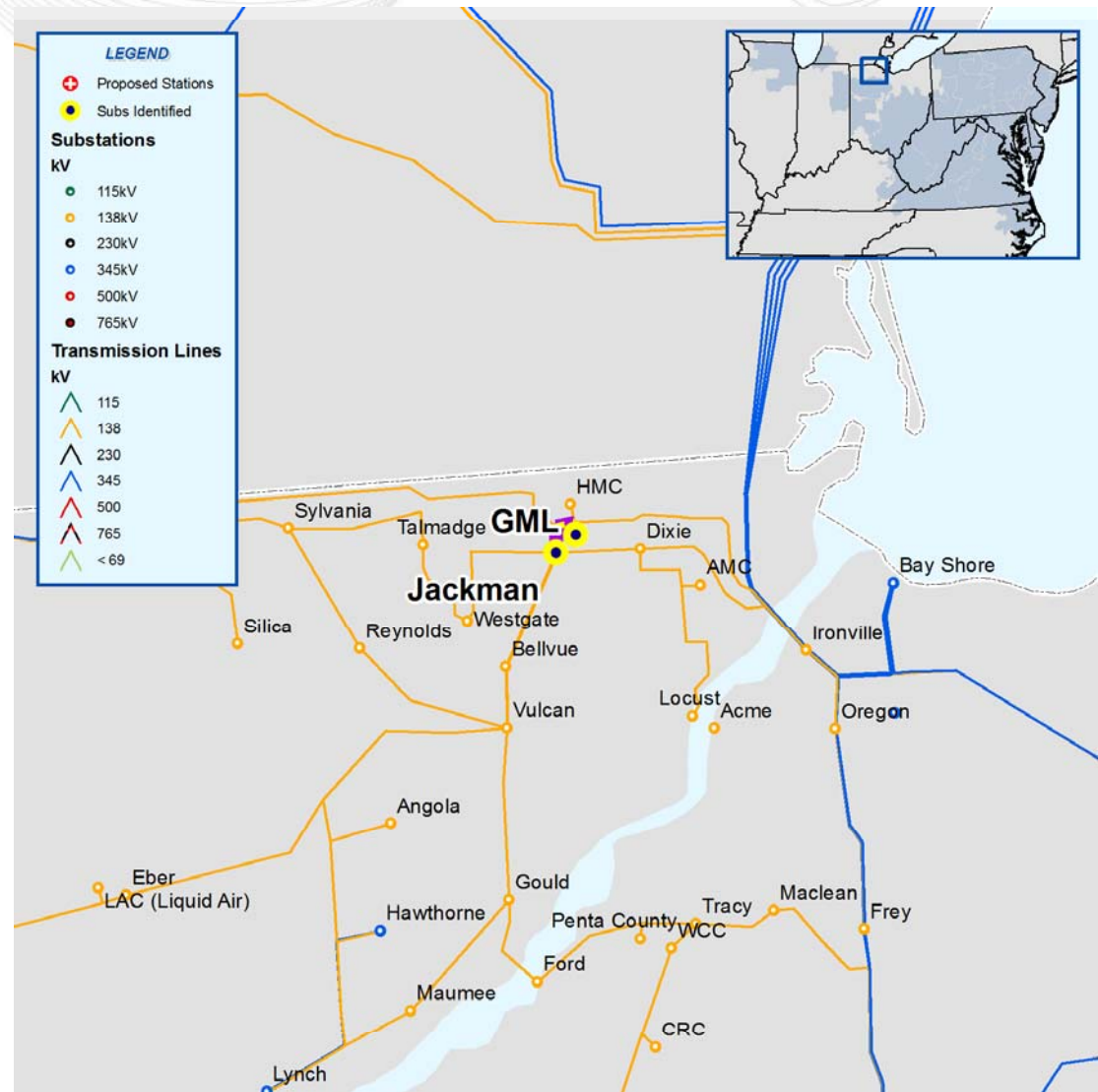
- For the common mode outage test the Bayshore – Chevy 138 kV circuit is overloaded for breaker failure operation of the Bayshore 138 kV BK-3K, BK-13254, BK-13256, BUS-K, BK-13252 or BK-KM breakers
- Recommended Solution: Reconductor Bayshore – Chevy 138 kV with 636 ACSS conductor (B1192)
- Estimated Cost: \$4.3M
- Expected In-Service Date: 06/01/2013



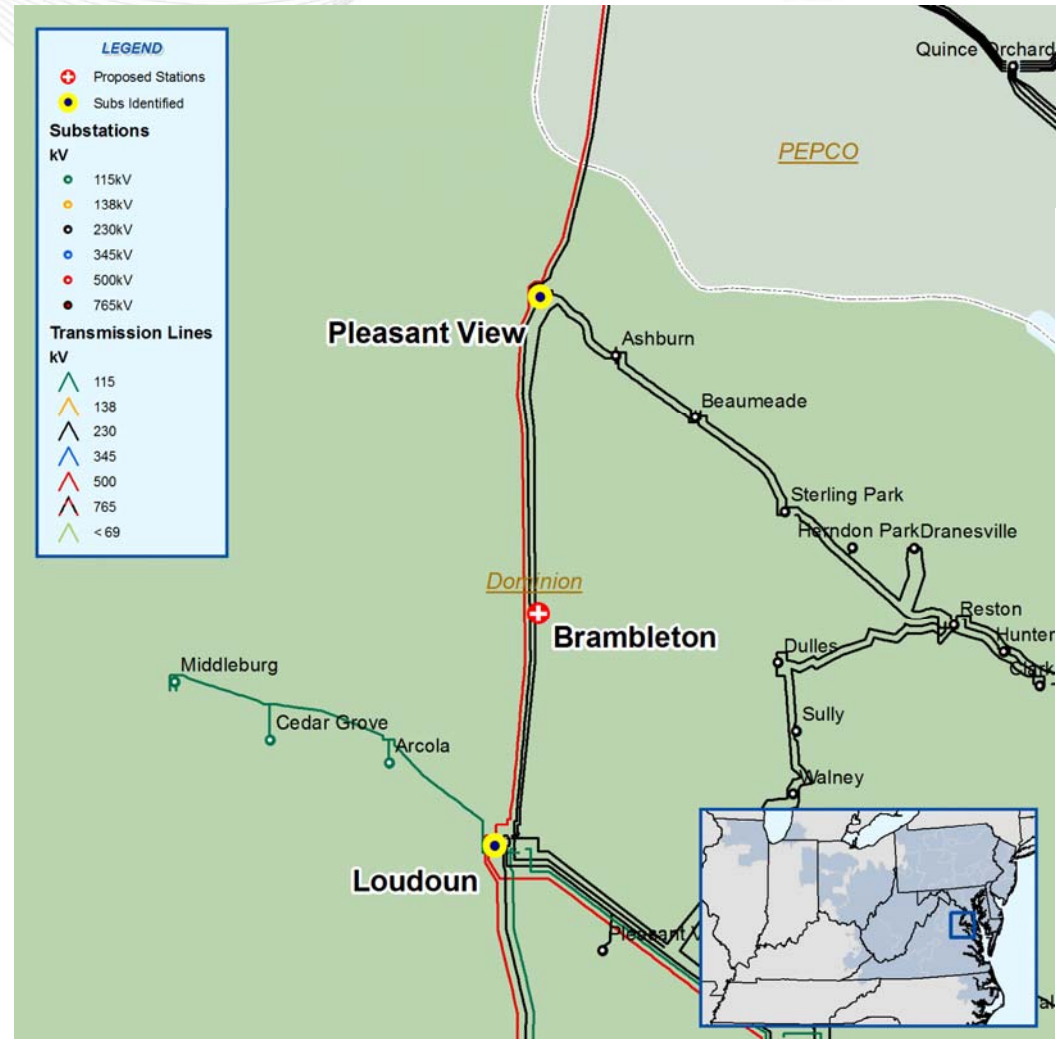
- For the common mode outage test the Hanna – East Akron 138 kV circuit is overloaded for breaker failure operation of West Ravenna 138 kV BK-15K and the tower outage of the Hanna – West Ravenna #1 and the Hanna – West Ravenna #2 138 kV lines
- Recommended Solution: Replace the 800 Amp wavetrap at East Akron with a 1200 Amp wavetrap (B1193)
- Estimated Cost: \$0.052M
- Expected In-Service Date: 06/01/2013



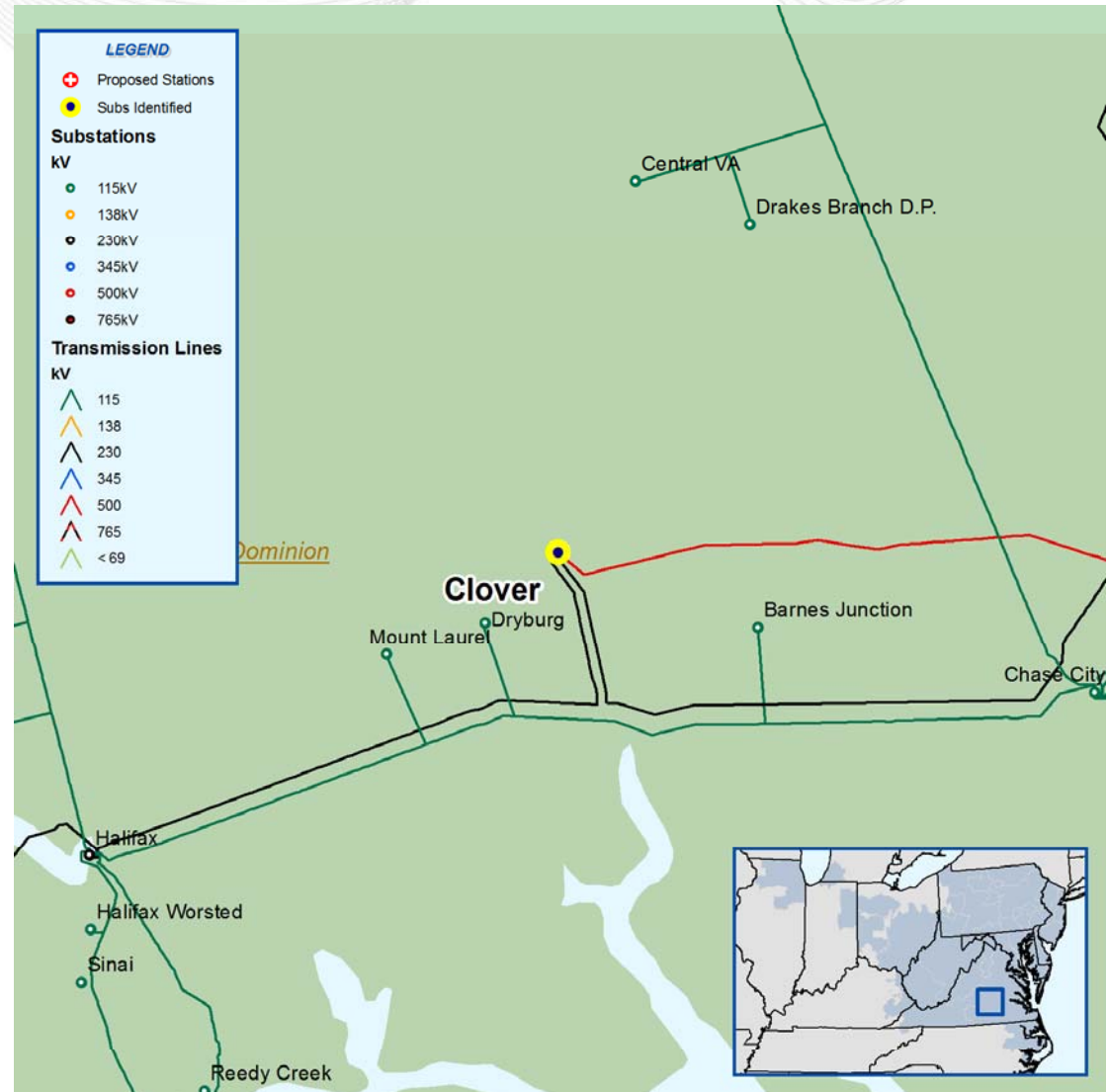
- For the common mode outage test the General Mills – Jackman 138 kV circuit is overloaded for the breaker failure operation of the Bayshore 138 kV BK-13254, BK-13256, BK-13252, BUS-K, or BK-KM breakers
- Recommended Solution: Reconductor General Mills – Jackman 138 kV with 636 ACSS conductor (B1194)
- Estimated Cost: \$0.647M
- Expected In-Service Date: 06/01/2013



- For Dominion and PEPCO Load Deliverability the Pleasant View 500/230 kV transformer is overloaded for the outage of Doubs to Brighton 500 kV and one Loudoun 500/230 kV transformer overloads for the outage of the parallel transformer
- Recommended Solution: Install Brambleton 500/230 kV transformer and associated breakers
- Estimated cost: \$18 M
- Expected In-service: 06/01/2014



- For Dominion Load Deliverability the Clover 500/230 kV transformer is overloaded for the outage of the Carson to Wake 500 kV line along with low voltages in the Clover area
- Recommended Solution: Install 2<sup>nd</sup> Clover 500/230 kV transformer and a 150 MVAR capacitor
- Estimated cost: \$16 M
- Expected In-service: 06/01/2015





# Review Issues Tracking

- **Alternative Analysis**
  - Combinations of alternatives, transmission, and reactive upgrades
  
- **Interim TEAC meeting to discuss progress**
  - Week of Wednesday, May 26th ?