

PJM DESIGNATED ENTITY DESIGN STANDARDS

1.0 PURPOSE

These ~~design criteria standards have been~~ establish ~~designed as a minimum design standard~~ ~~criteria~~ to provide a minimum level of robustness such that a new competitively-solicited facility will not introduce a weak point in the system in terms of performance. ~~These minimum design standards do not apply to projects for which solutions are not solicited through the PJM competitive process.~~

Comment [TDP1]: Suggest striking. The sentence is duplicated in the scope.

2.0 SCOPE

This document sets forth the minimum requirements for the design of overhead electric transmission line facilities rated 69kV and above for projects solicited through the PJM competitive process. These minimum design standards do not apply to projects not associated with the PJM competitive process.

3.0 GENERAL REQUIREMENTS

The design of all transmission lines shall meet or exceed the requirements of this document, the National Electrical Safety Code (ANSI/IEEE C-2) [NESC] in effect at the time of the project design, and all additional legislated requirements as adopted by governmental jurisdictions. It shall be the responsibility of the Designated Entity to identify all additional legislated requirements. In the event of conflicts between documents, the most stringent requirement shall apply.

4.0 CONDUCTOR

The Designated Entity shall determine normal and emergency ratings for both summer and winter seasons using an appropriate facility rating methodology. The Designated Entity shall provide documentation of the calculation method, including all assumptions for the input parameters. The conductor selected shall be compatible with all ampacity ratings.

Comment [TDP2]: Since line rating is out of scope, is this paragraph appropriate?

The loss of strength of the conductor shall be limited to 10% of its initial rated breaking strength for an assumed 35 year life. Conductor connectors and accessories shall have mechanical strength and thermal capabilities compatible with no less than the conductor.

Comment [TDP3]: Mechanical strength is 95%

The damaging effects of Aeolian vibration shall be appropriately mitigated ~~during the wire selection and design process.~~ Mitigation measures may include lower design tensions, mechanical vibration dampers, and spacer dampers for bundled conductor.

5.0 LOADING AND STRENGTH REQUIREMENTS

Transmission Line Facilities shall have sufficient strength to resist the individual and cumulative effects of all load cases defined in Section 5.1, including all subsections. The applied loads shall be adjusted by the Load Factors defined in the subsections of Section 5.1, and the material strengths shall be adjusted by the material strength reduction factors specified by the applicable governing industry ~~body publications~~ referenced in Section 5.2.

Transmission Line Facilities include all supporting structures, conductors and other wires, insulators, hardware, and foundations.

Comment [TDP4]: "conductors" – PECO comment; added other wires for completeness.

5.1 Design Load Requirements

All Transmission Line Facilities shall be designed to withstand the independent load cases defined in Sections 5.1.1 through 5.1.7. The effects of gravity, wind, ice, wire tension, construction, and maintenance loads shall be included as applicable.

5.1.1 Legislated Loads

5.1.1.1 Transmission Line Facilities shall be designed to resist the loading conditions defined in Rules 250B, 250C, and 250D of the NESC. For Rule 250B, the provisions of Grade B construction and the Heavy loading district shall be applied. The provision of Rules 250C and 250D permitting the exclusion of structures less than 60 feet in height shall not apply.

5.1.1.2 The Designated Entity shall identify and design to all additional legislated requirements as adopted by governmental jurisdictions.

5.1.2 Extreme Wind

Transmission Line Facilities shall be designed to resist the wind loads corresponding to a 100 year mean recurrence interval (MRI) as defined in the latest edition of ASCE Manual of Practice (MOP) 74.

Wind pressures shall be calculated in accordance with the procedures of the latest edition of ASCE ~~Manual of Practice~~^{OP} 74, properly adjusted for structure shape, gust, and height. The Load Factor applied shall be a minimum of 1.0.

Wind loads shall be applied in the direction producing the maximum loading effect.

All wires shall be assumed intact.

5.1.3 Concurrent Ice with Wind

Transmission Line Facilities shall be designed to resist the ice loads resulting from freezing rain corresponding to a 100 year MRI and along with the associated concurrent wind loads as defined in the latest edition of ASCE MOP 74 ~~corresponding to a 100 year MRI~~.

Wind pressures shall be calculated in accordance with the procedures of the latest edition of the ASCE ~~Manual of Practice~~^{OP} 74, properly adjusted for structure shape, gust, and height. The Load Factor shall be a minimum of 1.0.

Wind loads shall be applied in the direction producing the maximum loading effect.

The weight of ice shall be considered 57 pounds per cubic foot. The temperature used shall be either the values specified or 32°F. The Load Factor shall be a minimum of 1.0.

All wires shall be assumed intact.

5.1.4 Heavy Ice

Transmission Line Facilities shall be designed to resist ice loads resulting from freezing rain, snow, and in-cloud icing as defined in Sections 5.1.4.1 through 5.1.4.4.

In each case, the weight of ice shall be considered 57 pounds per cubic foot, the temperature 0°F, and the wind speed 0 mph. The Load Factor shall be a minimum of 1.0. All wires shall be assumed intact.

5.1.4.1 Transmission Line Facilities shall be designed to resist the effects of a minimum of 1.0 inch radial ice resulting from freezing rain applied to all wires. Transmission Line Facilities designed for voltages 230kV and greater shall also meet the requirements defined in Sections 5.1.4.2, 5.1.4.3, and 5.1.4.4.

5.1.4.2 Transmission Line Facilities designed for voltages 230kV and greater and constructed in the following states/districts, or portions ~~of the state~~ Pennsylvania thereof, shall be designed to resist the effects of a minimum of 1.5 inches radial ice resulting from freezing rain applied to all wires.

- District of Columbia
- New Jersey
- Pennsylvania, within 100 miles of the coast of the Atlantic Ocean ~~coast~~
- Delaware, within 75 miles of the coast of the Atlantic Ocean
- Maryland, within 75 miles of the coast of the Atlantic Ocean

5.1.4.3 Transmission Line Facilities designed for voltages 230kV and greater and constructed in regions with a ground elevation greater than 1500 feet and less than 3000 feet above mean sea level shall be designed to resist the effects of a minimum of 1.25 inch radial ice resulting from freezing rain applied to ~~the all~~ wires. Greater values shall be considered in areas known to accumulate larger amounts of ice resulting from freezing rain, or are prone to in-cloud icing or accumulation of snow, ~~and~~ and when indicated by historical weather data or site-specific ice studies.

5.1.4.4 Transmission Line Facilities designed for voltages 230kV and greater and constructed in regions with a ground elevation greater than 3000 feet above mean sea level shall be designed to resist the effects of a minimum of 1.5 inch radial ice resulting from freezing rain applied to ~~the all~~ wires. Greater values shall be considered in areas known to accumulate larger amounts of ice resulting from freezing rain, or are prone to in-cloud icing or accumulation of snow, ~~and~~ and when indicated by historical weather data or site-specific ice studies.

5.1.5 Unbalanced Longitudinal Load Cases

Transmission Line Facilities designed for voltages 230kV and greater shall be designed to resist longitudinal loads due to broken wire and differential ice conditions as described in Sections 5.1.5.1 and 5.1.5.2.

Transmission Line Facilities designed for voltages less than 230kV may be designed to resist longitudinal loads due to broken wire and differential ice conditions as described in Sections 5.1.5.1 and 5.1.5.2.

5.1.5.1 Broken Wire Loading

For single conductor phase configurations of both single and multiple circuit structures, only one conductor or one shield wire shall be considered broken in each load case. Each wire shall be broken individually to ensure the maximum loading effect is determined for each component. For the design of suspension structures, the conductor tensions may be reduced by the effects of longitudinal insulator displacement.

For phase configurations with more than one sub-conductor of both single and multiple circuit structures, a minimum of one sub-conductor or one ground static wire shall be considered broken ~~in each load case. The Each conductor bundle with the phase shall be evaluated with one broken~~ sub-conductor(s) ~~broken shall be considered individually~~ to ensure the maximum loading effect is determined for each component. For the design of suspension structures, the insulator shall be considered to remain vertical.

Comment [TDP5]: If we change, check rest of document for other instances of the use of "ground" wire.

The minimum environmental load condition shall be 0.5 inches of ice, 40 mph wind, and 32°F. The Load Factor shall be a minimum of 1.0.

~~For the design of suspension structures, the conductor tensions may be reduced by the effects of longitudinal insulator displacement.~~

5.1.5.2. Differential Ice Loading

With all wires assumed intact, each conductor and shield wire on one side of the structure shall be loaded with 0.5 inch of radial ice and 40 mph wind at a temperature of 32°F. All conductors and shield wires on the other side of the structure shall be loaded with the specified wind only. The weight of ice shall be considered 57 pounds per cubic foot. The Load Factor shall be a minimum of 1.0.

For the design of suspension structures, the conductor tensions may be reduced by the effects of longitudinal insulator displacement.

5.1.6 Construction and Maintenance Loads

Transmission Line Facilities shall be designed to ~~meet all applicable~~ facilitate complying with OSHA requirements related to climbing and fall protection, and the provisions of this section.

5.1.6.1 Bound Stringing Block

Transmission Line Facilities designed for voltages greater than 230kV shall be designed to resist longitudinal loads simulating a bound stringing block.

With all wires assumed intact, any one shield wire or phase conductor (or all sub-conductors of any one phase) shall be assumed to bind in a stringing block during installation. The block is assumed to swing 45° in-line. ~~Apply~~ The wind load shall be 2 pounds per square foot ~~of wind loading and with~~ no ice at a temperature of 30°F. The Load Factor shall be a minimum of 1.5.

5.1.6.2 Climbing and Working Loads

~~Structures Members of structures~~ shall be designed to support a point load of 350 pounds ~~at all areas~~ to accommodate construction or maintenance activities.

5.1.7. Foundation Loading

Foundation reactions shall be determined from the load cases presented in Section 5.1. Load Factors shall be a minimum of 1.0.

5.2 Strength Requirements

Transmission Line facilities shall ~~be designed for sufficient~~ meet the strength ~~as requirements~~ specified in Sections 5.2.1 through 5.2.3.

5.2.1 Strength Design Standards & Guides

Structures and foundations shall be designed to the requirements of the applicable publications:

- *ASCE Standard No. 10, Design of Latticed Steel Transmission Structures*
- *ASCE Standard No. 48, Design of Steel Transmission Pole Structures*
- *ASCE Manual No. 91, Design of Guyed Electrical Transmission Structures*
- *ASCE Manual No. 74, Guidelines for Electric Transmission Structural Loading*
- *ASCE Manual No. 104, Recommended Practice for Fiber-Reinforced Polymer Products for Overhead Utility Line Structures*
- *ASCE Manual No. 123, Prestressed Concrete Transmission Pole Structures*
- *ANSI 05-1, Specifications and Dimensions for Wood Poles*
- *IEEE Std. 691, Guide for Transmission Structure Foundation Design and Testing*

- IEEE Std. 751, Trial-Use Design Guide for Wood Transmission Structures
- ACI 318 Building Code Requirements for Structural Concrete and Commentary

5.2.2 Line Cascading Mitigation

To avoid cascading failures, structures shall be designed to withstand the unbalanced longitudinal load cases of Section 5.1.5, or an anti-cascading structure shall be placed every 5 miles.

5.2.3 Geotechnical Requirements

A geotechnical investigation shall be the basis of the final foundation design parameters.

6.0 ELECTRICAL DESIGN PARAMETERS

Conductor selection and configuration, including conductor size and the number of sub-conductors, shall consider electrical system performance parameters such as voltage, stability, losses, impedance, corona, electric and magnetic fields, audible noise, and ~~TV-television~~ and ~~Radio-radio~~ interference. To correct for voltage imbalance, the phases may be transposed.

The estimated levels of audible noise and EMF values shall not exceed those required by governmental jurisdictions. These estimated values shall be determined by calculations specific to the proposed transmission facility.

7.0 RIGHT-OF-WAY

Rights of way shall be proportioned so that NESC horizontal clearances to buildings are maintained at the edges. Consideration shall also be given to existing and future use of the area beyond their boundaries. Widths shall be calculated with the wires displaced from rest by a 6 psf wind at 60°F with no ice, ~~and~~ at final sag. Deflection of flexible structures and insulator swing shall be considered where appropriate. The Designated Entity shall ensure that the right of way width meets their Vegetation Management clearance guidelines to ensure compliance with NERC FAC-003 requirements.

Consideration shall be given to acquiring uniform right of way widths.

8.0 INSULATION, LIGHTNING PERFORMANCE, & GROUNDING

~~Insulation, grounding, and shielding of the transmission system (line and station) shall be coordinated between the Designated Entity and the Transmission Owner(s) to which the project interconnects to promote acceptable facility performance. The resulting design shall approach the targeted lightning performance defined below.~~

The Designated Entity shall specify transmission line insulation levels that promote the ~~safe and~~ reliable operation of the line(s) under normal operation and surge events. Shielding and grounding shall be ~~coordinated designed~~ by using an appropriate analysis method ~~to such~~

Comment [TDP6]: SPP wording, modified terminology to match PJM's, and expanded to incorporate the targeted performance. Suggest replacing the next paragraph with this.

Comment [TDP7]: Suggest striking "safe". Too hard to quantify and measure. And the NESC (Rule 273) specifies minimum insulation levels.

~~that verify that the line design will result in~~ the following targeted lightning performance ~~is~~ approached.

Comment [TDP8]: Suggested rewording if the other proposal (previous paragraph) is not acceptable.

- Voltages 345kV and greater – 1 Outage/100 circuit miles/Year
- 230kV – ~~1-2~~ Outage/100 circuit miles/Year
- 138/115kV – ~~1-3~~ Outage/100 circuit miles/Year
- 69kV – ~~1-4~~ Outage/100 circuit miles/Year

Comment [TDP9]: The new TSS document proposes 3, but 4 seems more realistic for 69kV.

Surge arresters, if installed, shall be applied in a manner that reduces the likelihood that the arrester or any of its associated hardware will interfere with reliable normal operation of the line in the event of surge arrester electrical or mechanical failure.

9.0 CLEARANCES

9.1 General

Unless otherwise stated, all clearances shall meet or exceed those defined in the NESC.

Clearances shall be maintained applying the maximum operating voltages ~~as~~ defined in PJM Manual 3, "Baseline Voltage Limits", Exhibit 3, Section 3.3.1. The circuit transient overvoltage (TOV) shall be used when considering the alternate clearances permitted by NESC Rules 232D, 233C3, 234H, 235B3.

~~For conductor-to-conductor clearances between different circuits and where~~ When the line is proposed transmission line under design is crossing over an existing supply or communication line, the position of the lower conductor wire position shall be determined by a straight line between ~~conductor~~ attachment points, unless specific sag/tension information for the lower ~~conductors/cables/wires~~ are known. When the sag/tension characteristics of the lower ~~conductors/cables/wires~~ are known, the ~~conductor~~ environmental requirements of the NESC rules may be applied.

Comment [TDP10]: Do we mean environmental loading characteristics.

9.2 Live Line Maintenance Requirements

Adequate clearances shall be provided when live-line maintenance requirements are specified for a line design for any of the following maintenance activities:

- Climbing inspection
- Hot stick maintenance for the specified line components
- Live line maintenance for the specified line components using specified lift equipment
- Helicopter live line maintenance for the specified line components using the specified helicopter

All live line maintenance clearances shall be determined using the OSHA calculation methods for the specified circuit TOV, ~~and~~ breaker design, and maintenance program.

9.3 Vertical Clearances

The vertical conductor clearances of Section 23 of the NESC shall be maintained at the NESC stated conditions ~~unless modified in Sections 9.5~~. All terrain points under the conductors shall be considered to be traversable by vehicles accessible. The buffers defined in Section 9.5 shall be applied.

9.4 Horizontal Clearances

The horizontal conductor clearances of Section 23 of the NESC shall be maintained at the NESC stated conditions. ~~The buffers defined in Section 9.5 shall be applied unless modified in Sections 9.5~~.

9.5 Clearance Buffers

Due to uncertainties and inaccuracies in surveying and installation of foundations, structures and conductors, the calculated position of the conductors shall be increased as buffers defined specified in Sections 9.5.1 and 9.5.2 ~~shall be added to clearances specified in section 23 of the NESC~~.

Comment [TDP11]: The way this is written, we are requiring that our clearances meet or exceed NESC + 3'. But in practice, what we all do (or what I think we all do) is to add the 3' (or some other number) to account for uncertainties and inaccuracies so that in the end, we meet NESC clearances. If we extend our clearances by 3', do we need to add another buffer now to account for these (uncertainties)?

9.5.1 Vertical Clearance Buffer

The vertical clearance buffer shall be 3'-0".

9.5.2 Horizontal Clearance Buffers

The horizontal clearance buffer shall be 2'-0".

9.6 Electrostatic Clearance

The short circuit current discharge requirements of NESC Rule 232D3(c) shall be met.

9.7 Agricultural Clearances

In ~~land areas that may utilize farm~~ farmlands, additional conductor clearances shall be provided in accordance with NESC Table 232-1 footnote 26.

9.8 Clearances over Waters of the United States

Clearances over the waters of the United States shall be the larger of the NESC requirements in Rule 232, or the clearance determined by the Army Corps of Engineers, plus the buffer defined in Section 9.5.

9.9 Galloping

9.9.1 General

Lines shall be designed to limit the likelihood that conductor/shield wire galloping will result in a circuit momentary operation. Galloping shall be addressed by one or a combination of the following methods:

- Performing a study which demonstrates that the route traversed by the line is not likely to be prone to the wind/ice conditions attributed to conductor galloping.
- Providing conductor clearances at the structure which produce the in-span conductor clearances defined below in Section 9.9.3.
- Install in-span interphase insulators or anti-galloping devices designed to reduce the possibility and/or severity of conductor galloping.
- Install twisted pair conductor.

Comment [TDP12]: PECO

9.9.2 Galloping Ellipse Calculations

Conductor galloping ellipses shall be developed using ~~either a combination of~~ the A.E. Davison method for single loop galloping and the L.W. Toye method for double loop galloping, or the CIGRE method ~~per as described in~~ Bulletin 322. The following load cases shall be used for galloping calculations for ~~either all~~ stated methods:

- 32°F, 0.5" Radial ice, 2 PSF pounds per square foot wind (~~For for~~ determination of Swing Angle)
- 32°F, 0.5" Radial ice, No Wind (For determination of sag and conductor motion ellipses)

Single loop galloping shall be used for spans less than 700 feet. Double loop galloping shall be used for spans of 700 feet or greater or any span where the conductor has dead-end terminations on both ends.

~~Long For long~~ spans over eighteen hundred (1800) feet, ~~shall take into account~~ existing line historical operation shall be considered. If no data is available, a study shall be performed to determine the proper mitigation methods.

9.9.3 Galloping Clearances

~~The conductor c~~clearances of the calculated galloping ellipses requirements shall meet the requirements of Sections 9.9.3.1 and 9.9.3.2.

9.9.3.1 Single Loop Galloping

The ~~major axes~~ position of the calculated galloping ellipses shall overlap no more than 10%.

Comment [TDP13]: Is it the major axis, or the ellipse itself?

9.9.3.2 Double Loop Galloping

The calculated positions of the galloping ellipses shall not overlap.

~~When galloping mitigation devices are used, greater overlap of galloping ellipses is permitted. Greater overlap in the calculated positions of galloping ellipses is permitted when galloping mitigation devices are used.~~

9.10 Avian Considerations

The Designated Entity shall comply with all project-specified requirements established by governmental jurisdictions. The guidelines of the Avian Power Line Interaction Committee shall be considered in the design of Transmission Line Facilities.